APPENDIX A

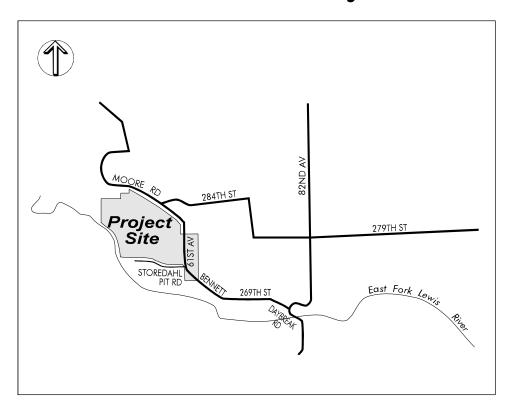
Daybreak Mine: Transportation Impact Study

Daybreak Mine

Transportation Impact Study

Prepared for

Clark County



Prepared by

DKS Associates

August 1998

1400 SW 5th Avenue, Suite 500 Portland, OR 97201 Phone: (503) 243-3500 Fax: (503) 243-1934

August 21, 1998

Richard Gamble, Clark County Public Works 1300 Ester Vancouver, WA 98666-9810

Subject: Daybreak Mine Transportation Impact Study P98201x0

Dear Richard:

Attached is the revised transportation impact study for the Daybreak Mine expansion in Clark County. I have included the information you requested per the Transportation Impact Study Technical Complete Checklist dated 8/14/98. Information added to this report includes:

- ADT at study intersections (see appendix)
- Accident rates and calculations (see report section and appendix)
- Trip Generation data and calculations (see appendix)
- Future (1999) Base traffic volumes (see Figure 7)
- Future (1999) Base LOS (see Table 4)

Please call me if you have any questions.

Sincerely,

DKS Associates A Corporation

Brian K. Copeland, P.E. Transportation Engineer

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1. Summary

J.L. Storedahl & Sons is proposing to expand their existing Daybreak Mine in eastern Clark County. The Daybreak Mine is located just west of 61st Avenue and Bennett Road on the north side of the East Fork Lewis River (Figure 1). Access to the Daybreak Mine would continue to be off Bennett Road/61st Avenue as it is today. This report evaluates the traffic and transportation impacts for the proposed Daybreak Mine expansion.

Existing Conditions

Based on the Clark County Transportation Impact Study Procedures, the following intersections were selected for focused analysis in this report:

- NE JA Moore Road/NE 284th Street
- NE 61st Avenue/Bennet Road/Site Access
- NE Hyatt Road/NE Daybreak Road
- NE 82nd Avenue /NE 279th Street

All four unsignalized study intersections operate at acceptable level of service (LOS C or better) during both the AM and PM peak periods.

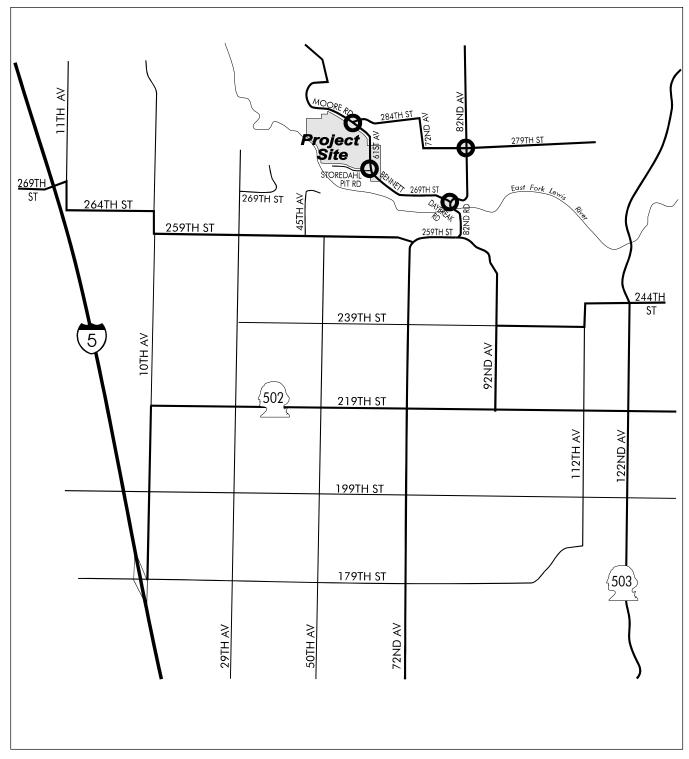
Accident rates at all four study intersections for the five year period are less than 1.0 accidents per million vehicles entering the intersection.

Impacts

Presently, about 4,000 tons of rock per day are currently exported from Daybreak Mine during peak operations¹. Approximately 5,000 tons per day are currently imported from the Tebo Pit southwest of the Daybreak site during peak operations. No mining is currently being conducted at the Daybreak site. The majority of imports and exports are hauled in 30-ton trucks. The exception to this is that cash sales, which represent about 15 percent of exports, are hauled in various smaller trucks. The average load for a cash sale is approximately eight tons. The projected export volume is approximately 8,000 tons of rock per day during peak operations.

Information provided to DKS in a letter from Skip Urling, Ecological Landscape Services, Inc. on 7/21/98.





LEGEND

O - Study Intersection

Figure 1 STUDY AREA

The projected volume of material imported into the site for processing will drop to about 2,500 percent.

Daybreak plans to mine approximately 4,000 tons of rock per day during peak operations and transfer this rock to the processing area by use of an on-site conveyor system. This alternative will be referred to as Alternative 1 in this report. Although using this conveyor system is the preferred plan, an alternative to this would be to transfer the 4,000 tons of rock per day along NE 61st Avenue/Bevin Road via a series of existing driveways north of the main site access. This alternative will be referred to as Alternative 2 in this report. Although three access points would be needed for Alternative 2, only one would be utilized at a time. No change in on-site employment is planned for either alternative.

Cash sales would continue to comprise approximately 15 percent of export volume. If the conveyor system is not used (Alternative 2), cash sales would be restricted until after 9:00 am to reduce vehicle trips generated during the morning peak hour.

For Alternative 1, the proposed Daybreak Mine operation is expected to generate about 23 additional vehicle trips during the AM peak hour and about 12 vehicle trips during the PM peak hour. For Alternative 2, the proposed Daybreak Mine operation is expected to generate about 28 additional vehicle trips during the AM peak hour and about 30 vehicle trips during the PM peak hour. These numbers are based on the busiest time of the year and, therefore, represent a peak estimate of trip generation.

All four study intersections would operate at acceptable levels of service (LOS C or better) for both alternatives under both Existing (1998) Plus Project and Future (1999) Plus Project scenarios.

For Alternative 1, sight distance (both directions) at the access point more than meets the required 500 feet minimum. Figures showing sight distance requirements for both Alternatives 1 and 2 are shown in the appendix of this report.

Mitigation

In general, there are few traffic impacts created by the proposed project. Measures which can be undertaken to reduce the potential concerns regarding truck traffic would include the following:

- Improved street lighting at site driveways to improve nighttime visibility in winter conditions.
- Work with school districts to identify school bus stop areas for children and provide widened shoulder areas (where needed or not already provided) on key routes in the study area.

2. Existing Conditions

This section summarizes the existing transportation conditions in the vicinity of the proposed project, including roadway geometries, traffic volumes, vehicle speeds, and pedestrian, bicycle and transit facilities. Existing operating conditions of roadways and key intersections in the study area are also discussed.

Based on the Clark County traffic studies scoping² letter for this project, the following four intersections were selected for focused analysis in this report:

- NE JA Moore Road/NE 284th Street
- NE 61st Avenue/Bennet Road/Site Access
- NE Hyatt Road/NE Daybreak Road
- NE 82nd Avenue/NE 279th Street

EXISTING NETWORK DESCRIPTION

Regional access to the project site would be provided via I-5 and I-205. Main access to the Daybreak Pit would be provided off Bennett Road/61st Avenue. Three additional access points will be provided north of this primary access point for purposes of transferring mined aggregate to the processing facility. The following sections describe the key arterial routes and freeways which would serve the proposed project.

NE Daybreak Road/NE 82nd Avenue (south of Hyatt Road) is a two-lane, north-south roadway identified as a Major Rural Collector by Clark County. This road is about 24 feet wide and provides a connection between 269th Street and 72nd Avenue. The posted speed along 82nd Avenue is 25 mph between 72nd Avenue and 269th Street. No bike lanes or sidewalks are provided along the roadway.

NE 269th Street/NE Bennett Road/NE 61st Avenue/NE Bevin Road/NE Moore Road is a two-lane, east-west road designated a Major Rural Collector by Clark County. In the vicinity of the existing Daybreak Pit, 269th Street becomes Bennett Road east of the pit's access road and west of the

Based on traffic studies scoping letter from Richard Gamble of Clark County dated May 26, 1998.

Daybreak Park. At the pit's access road, Bennett Road then becomes 61st Avenue running north-south. 61st Avenue then turns into Bevin Road, which turns into Moore Road at 284th Street. This roadway is 22-24 feet wide and provides the only direct connection between the Daybreak Mine site and 72nd Avenue and State Route 502. The posted speed along this road is 40 miles per hour for trucks (along 269th Avenue), with a posted speed of 35 miles per hour at various curves along the roadway. No bike lanes or sidewalks are provided along the roadway. Several school bus stops are located along this roadway. 269th Avenue is controlled by a stop sign at Hyatt Road. (The only traffic expected to go north on 61st Avenue from the pit are trips between Storedahl's operation in Woodland, Washington and the Daybreak Pit. The level of activity between these two facilities would be the same as it is today (without crushing activity at Daybreak).)

NE Hyatt Road is a two-lane roadway connecting NE Daybreak Road with NE 82nd Avenue. It is classified as a Major Rural Collector by Clark County. The roadway is approximately 22 feet wide, with no bike lanes or sidewalks. The posted speed along Hyatt Road is 25 miles per hour for trucks due to curves and steep grades. A school bus stop is located along Hyatt Road.

NE 82nd Avenue (north of Hyatt Road) is a two-lane roadway classified as a Major Rural Collector by Clark County. The roadway is approximately 22 feet wide, with no bike lanes or sidewalks. Sharp curves in the roadway are posted at 20 miles per hour.

NE 284th **Street** is a two-lane roadway classified as a Major Rural Collector by Clark County. The roadway is approximately 20 feet wide with no bike lanes or sidewalks. 284th Street is controlled by a stop sign at Moore Road. The posted speed is 20 miles per hour due to curves ans steep grades.

NE 279th **Street** is a two-lane roadway classified as a Major Rural Collector by Clark County. The roadway is approximately 20 feet wide with no bike lanes or sidewalks. It is controlled by a stop sign at 82nd Avenue. The posted speed along 279th Avenue is 35 miles per hour west of 82nd Avenue.

INTERSECTION CAPACITY

Analysis of traffic volumes is useful in understanding the general nature of traffic in an area, but by itself indicates neither the ability of the street network to carry additional traffic nor the quality of service afforded by the street facilities. For this, the concept of *level of service* has been developed to subjectively describe traffic performance.

Level of service categories are similar to report card ratings for traffic performance. Intersections are typically the controlling bottlenecks of traffic flow and the ability of a roadway system to carry traffic efficiently is generally diminished in their vicinities. Levels of Service A, B and C generally indicate conditions where traffic moves without significant delays over periods of peak travel demand. Level of service D and E indicate progressively worse peak hour operating conditions and level of service F conditions occur when demand exceeds the capacity of an intersection. Most urban communities set level of service D as the minimum acceptable level of service for peak hour operation and plan for level of service C or better for all other times of the day. The minimum acceptable level of service for rural areas of Clark County is LOS C.³ Level of service descriptions for unsignalized intersections are provided in the appendix of this report.

Unsignalized intersection level of service is reported for the major street and minor street (generally, left turn movements). The method assesses available and critical gaps in the traffic stream which make it possible for side street traffic to enter the main street flow. The 1994 Highway Capacity Manual describes the detailed methodology. It is not unusual for an intersection to experience level of service E or F conditions for the minor street left turn movement. It should be understood that, often, a poor level of service is experienced by only a few vehicles and the intersection as a whole operates acceptably.

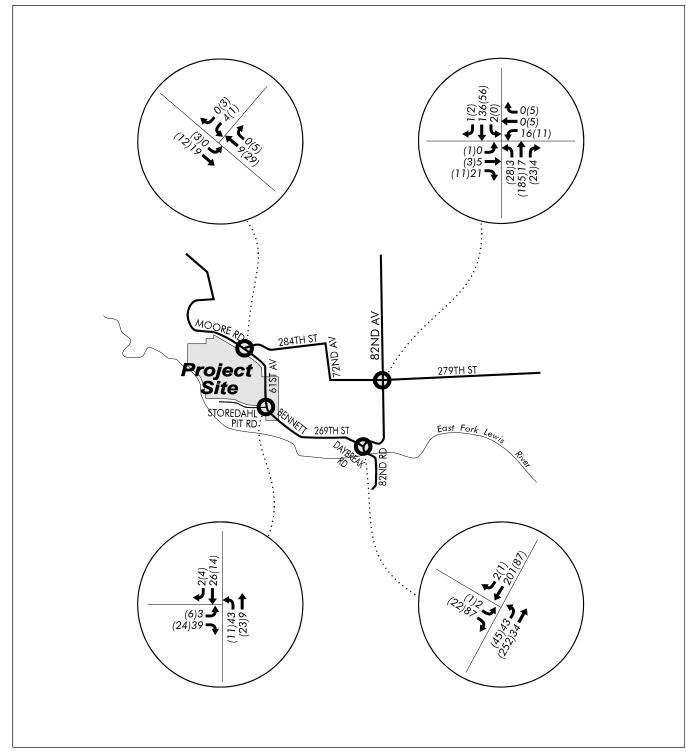
Intersection turn movement counts were conducted at the four study intersections during the morning (7:00-9:00 AM) and evening (4:00-6:00 PM) peak periods to determine existing LOS based on the 1994 Highway Capacity Manual methodology for signalized and unsignalized intersections⁴.

Traffic counts were conducted from June 29 to July 1, 1998. Figure 2 provides a summary of the existing traffic volumes. The results of the intersection analysis are shown in Table 1. All four study intersections are currently unsignalized. As shown in Table 1, all study intersections operate at acceptable level of service (LOS C or better) during both the AM and PM peak periods.

Based on discussion with Clark County staff on March 27, 1996.

⁴ - Highway Capacity Manual, Special Report 209, Transportation Research Board, Chapter 10, 1994.





LEGEND

O - Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 2
EXISTING PEAK HOUR
TRAFFIC VOLUMES

Table 1
Existing (1998) Intersection Operation

	AM Pea	ak Hour	PM Pe	eak Hour
Intersection	Delay	LOS	Delay	LOS
NE JA Moore Road/NE 284 th Street	0.4	A/A	0.3	A/A
Bennet Road/61st Avenue/Site Access	2.0	A/A	1.5	A/A
NE Hyatt Road/NE Daybreak Road	1.5	A/A	0.6	A/A
NE 61 st Avenue/NE 82 nd Avenue	0.9	A/A	0.7	A/B

Unsignalized Intersection LOS:

A/A = Major street left turn LOS/minor street left turn LOS

Delay = Average vehicle delay in peak hour for entire intersection

BENNETT ROAD SPEED SURVEY

A 24-hour speed survey was conducted along Bennett Road just south of the main Daybreak Mine access (Storedahl Pit Road). The 85th percentile speed was 51 miles per hour in the northbound direction and 48 miles per hour in the southbound direction. By definition, 15 percent of the vehicles surveyed were traveling faster than the 85th percentile speed and 85 percent of the vehicles surveyed were traveling slower than the 85th percentile speed.

ACCIDENT HISTORY

Based on accident data provided by Clark County, four accidents occurred within the study area during the five year period from 1992 through 1996⁵. Three of these accidents occurred at or near the intersection of NE 82nd Avenue/NE 279th street. The other accident occurred at the intersection of NE JA Moore Road and NE 284th Street. No fatalities were reported. Accident rates at all four study intersections for the five year period are less than 1.0 accidents per million vehicles entering the intersection. Accident rate calculations are shown in the appendix.

⁵ Based on fax from Huan Vuu, Clark County Public Works, on 7/2/98.

PEDESTRIAN/BICYCLE

During both the morning and evening peak periods, there were very few pedestrians observed in the vicinity of the project site. The only noticeable pedestrian activity observed along key routes is related to school children waiting for buses in the morning and returning in the afternoon. No pedestrian or bicycle facilities are provided along any of the study area roadways.

TRANSIT/BUS

The Battle Ground School District has two bus routes which pick up and drop off students along 269th Avenue near the proposed project site⁶. Bus #12 serves Lewisville Middle School and Battle Ground High School and bus #21 serves Chief Umtuch and Captain Strong primary schools. Both these bus routes travel along 269th Street/Bennet Road/61st Avenue, 284th Avenue, and 279th Avenue in the study area. Bus #12 also travels along 82nd Avenue north of Daybreak Road. The school district is currently modifying its routes, but the new routes were not available at the time of this study.

The La Center School District has one bus route in the vicinity of the project⁷. This route runs along 284th Street and 61st Avenue north of the Daybreak site, and along Bennet Road and 269th Street south of the Daybreak site. A bus turnaround is located along 269th Street at about 69th Avenue.

⁶ Based on discussion with Brenda Lester of Battle Ground Public Schools on 7/21/98.

Based on fax from Gladys Doriot, KWRL Transportation Co-op dated 7/14/98.

3. Impacts

This chapter reviews the impacts of the proposed Daybreak Mine on the study area transportation system. The analysis includes an assessment of project trip generation and distribution, capacity analysis of study intersections with existing and projected future traffic, sight distances evaluation, and pedestrian/bicycle access consideration.

Presently, about 4,000 tons of rock per day are exported from Daybreak Mine during peak operations (June through November), with approximately 1,500 tons of rock per day exported the remainder of the year⁸. An average of 4,500 tons of rock per day are currently imported from the Tebo Pit southwest of the Daybreak site. During peak operations, this number increases to approximately 5,000 tons per day. No mining is currently being conducted at the Daybreak site. The majority of imports and exports are hauled in 30-ton trucks. The exception to this is that cash sales, which represent about 15 percent of exports, are hauled in various smaller trucks. The average load for a cash sale is approximately eight tons.

Proposed on-site activities include mining, processing, sorting and stockpiling sand and gravel. The projected export volume is approximately 8,000 tons of rock per day during peak operations (June to October), with this number falling to about 3,000 tons/day the remainder of the year. The projected volume of material imported into the site for processing will drop to about 2,500 tons per day. This will reduce the amount of rock imported from the Tebo Pit by about 50 percent.

Daybreak plans to mine approximately 4,000 tons of rock per day during peak operations (average is 2,500 tons/day) and transfer this rock to the processing area by extending an existing on-site conveyor system. This alternative will be referred to as Alternative 1 throughout the remainder of this report. Although use of this conveyor system is the preferred plan, an alternative to this would be to transfer the 4,000 tons of rock per day along NE 61st Avenue/Bevin Road/JA Moore Road via a series of three existing driveways north of the current site access. This alternative will be referred to as Alternative 2 in this report. Although three access points would be needed for Alternative 2, only one would be utilized at a time. Site access will be discussed later in this report. No change in on-site employment is planned for either alternative.

⁸ Information provided to DKS in a letter from Skip Urling, Ecological Landscape Services, Inc. on 7/21/98.

Cash sales would continue to comprise approximately 15 percent of export volume. If the conveyor system is not used (Alternative 2), cash sales would be restricted until after 9:00 am to reduce vehicle trips generated during the morning peak hour.

Although the previous discussion includes rock volumes for average and off-season operation levels, the volumes during peak operations are used for analysis in this study to represent a worst-case scenario of vehicle and truck trips. With this in mind, the proposed project would do the following:

- Increase exported volume by about 4,000 tons per day
- Decrease imported volume from the Tebo Pit by about 2,500 tons per day
- Approximately 4,000 tons per day of raw material would be mined and transported to the processing area.

The following three scenarios will be evaluated in this section:

- Existing (1998) Plus Project (Alternatives A and B)
- Future (1999) Base
- Future (1999) Plus Project (Alternatives A and B)

TRIP GENERATION

The trip generation for the proposed Daybreak Pit was determined based on traffic counts⁹ conducted at the existing Daybreak Mine site access and information provided by J.L. Storedahl & Sons. The trip generation data used for this analysis represents a typical day during Daybreak's peak operating season. Trip generation data and supporting calculations are included in the appendix.

For Alternative 1, the proposed Daybreak Mine operation is expected to generate about 23 additional vehicle trips during the AM peak hour and about 12 vehicle trips during the PM peak hour. For Alternative 2, the proposed Daybreak Mine operation is expected to generate about 28 additional vehicle trips during the AM peak hour and about 30 vehicle trips during the PM peak hour. These numbers are based on the busiest time of the year and, therefore, represent a peak estimate of trip generation. Trip generation estimates for the Daybreak Pit are shown in Table 2.

Table 2

⁹ Traffic counts conducted by DKS Associates, June 30 1998.

Vehicle Trip Generation

	AM Peak Hour	PM Peak Hour
Alternative 1 (conveyor)	12 in/11 out	4 in/8 out
Alternative 2 (no conveyor)	15 in/13 out	11 in/19 out

TRIP DISTRIBUTION/ASSIGNMENT

Trip distribution was based on Clark County existing truck and traffic patterns in the study area, as well as information provided by J.L Storedahl & Sons. Added project vehicle trips are shown in Figure 3 and 4 for the two alternatives, along with the respective distribution percentages. Trips were assigned to the roadway network based on this distribution, and added project traffic was traced from the project site through the study intersections.

INTERSECTION CAPACITY

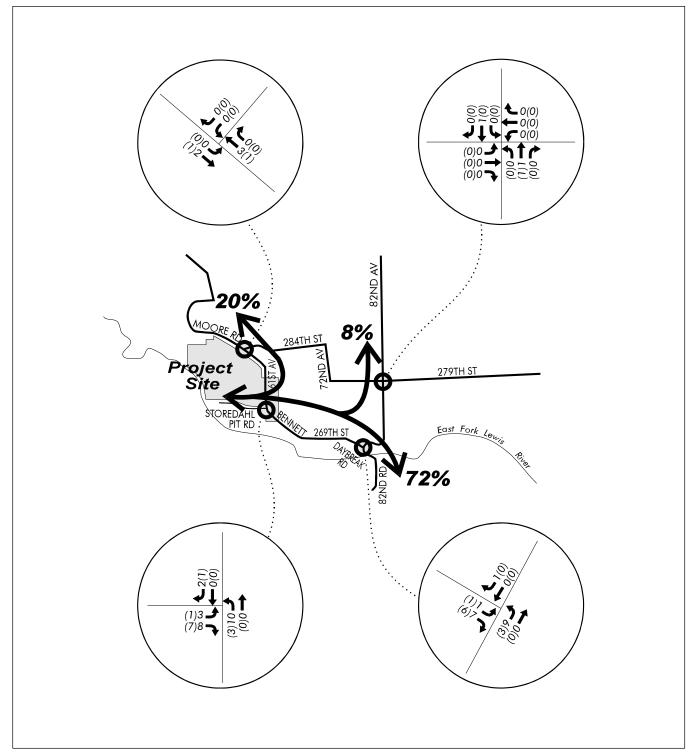
The following sections provide results of intersection capacity analysis for the three scenarios listed above. A description of each scenario is also included herein.

Existing (1998) Plus Project

This scenario provides the best indication of project-related impacts on the roadway system without other land use changes. Vehicle trips generated by the project were added to existing (1998) traffic volumes in the study area to arrive at "Existing Plus Project" traffic volumes. Figures 5 and 6 show estimated traffic volumes for this scenario for Alternatives 1 and 2, respectively.

Table 3 shows the resulting levels of service for the four study intersections for this scenario. As the table shows, all four study intersections would operate at acceptable levels (LOS C or better) during both AM and PM peak periods.





LEGEND

O - Study Intersection

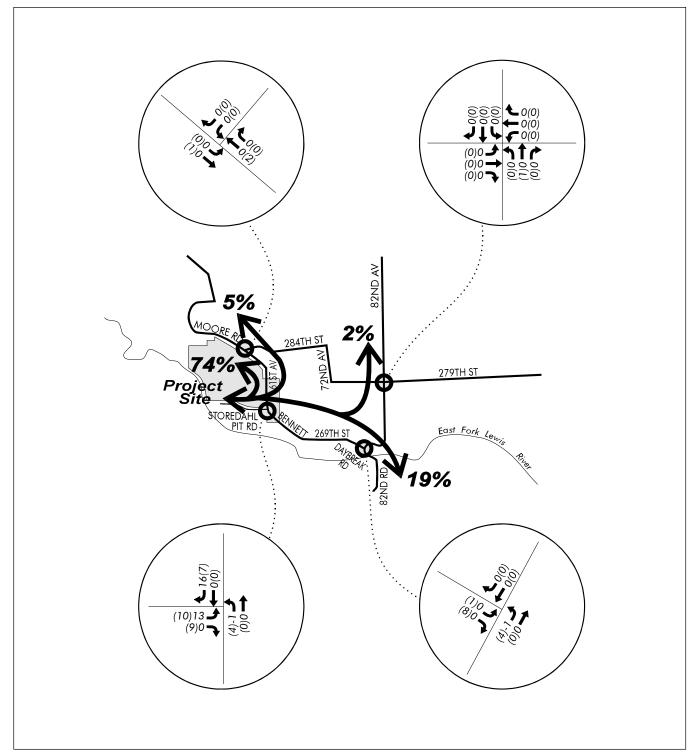
AM(PM) - Peak Hour Traffic Volumes

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Directional Distribution for Added Vehicle Trips

Figure 3
ADDED PROJECT TRAFFIC
ALTERNATIVE 1 (Conveyor)





LEGEND

Study Intersection

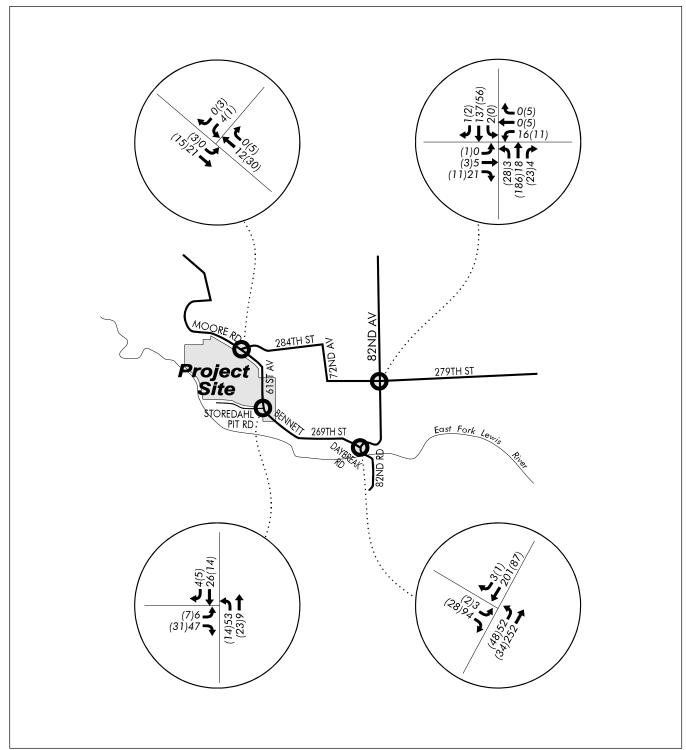
AM(PM) - Peak Hour Traffic Volumes

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Directional Distribution for Added Vehicle Trips

Figure 4
ADDED PROJECT TRAFFIC
ALTERNATIVE 2 (No Conveyor)





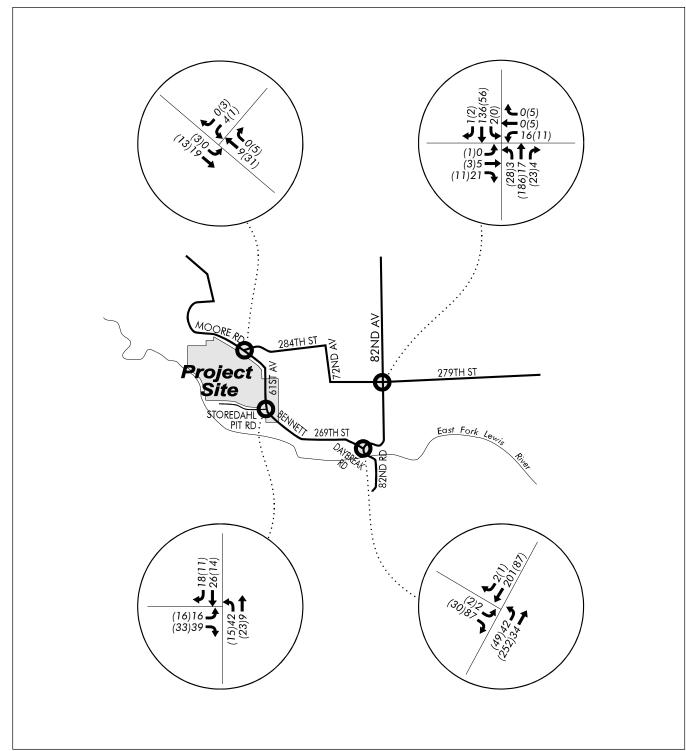
LEGEND

Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 5
EXISTING PLUS PROJECT
ALTERNATIVE 1 (Conveyor)





LEGEND

Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 6
EXISTING PLUS PROJECT
ALTERNATIVE 2 (No Conveyor)

Table 3
Existing (1998) Plus Project Intersection Operation

	The second secon	AM Pea	k Hour	PM Pea	ak Hour
	Intersection	Delay	LOS	Delay	LOS
Alternative 1	NE JA Moore Road/NE 284 th Street	0.4	A/A	0.3	A/A
(conveyor)	Bennet Road/61st Avenue/Site Access	2.1	A/A	1.6	A/A
	NE Hyatt Road/NE Daybreak Road	1.7	A/A	0.6	A/A
	NE 82 nd Avenue/NE 279 th Street	0.9	A/A	0.7	A/B
Alternative 2	NE JA Moore Road/NE 284th Street	0.4	A/A	0.3	A/A
(no conveyor)	Bennet Road/61st Avenue/Site Access	2.0	A/A	1.8	A/A
	NE Hyatt Road/NE Daybreak Road	1.5	A/A	0.6	A/A
	NE 82 nd Avenue/NE 279 th Street	0.9	A/A	0.7	A/B

Unsignalized Intersection LOS:

A/A = Major street left turn LOS/minor street left turn LOS

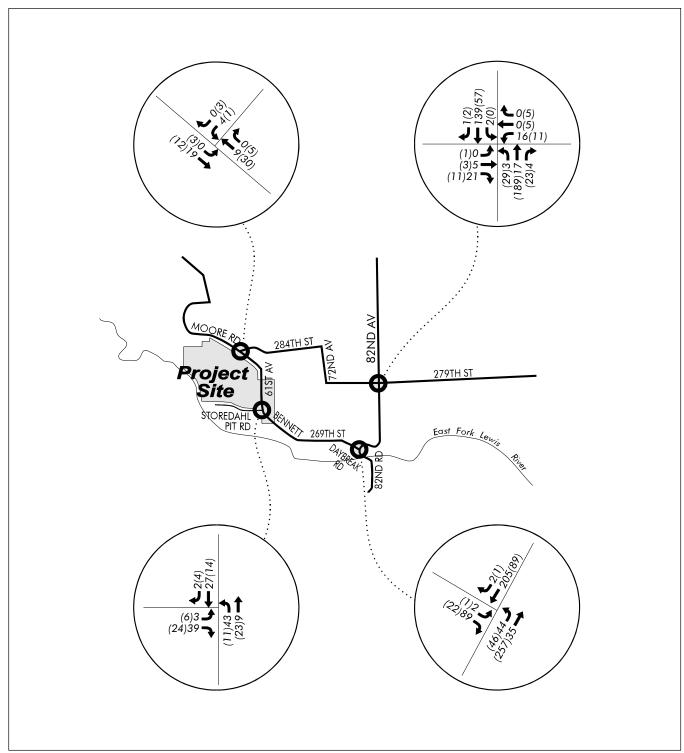
Delay = Average vehicle delay in peak hour for entire intersection

Future (1999) Base

For this study, it is assumed that the proposed Daybreak Mine operation would be in effect sometime in the year 1999. To obtain 1999 base traffic volumes, existing (1998) traffic volumes were factored up to represent base conditions one year into the future ¹⁰. The roadway network and geometries were assumed to remain the same as those for the existing case. Future (1999) Base traffic volumes are shown in Figure 7, and resulting intersection levels of service for the four study intersections are shown in Table 4. As shown in Table 4, all four study intersections would operate at acceptable levels (LOS C or better) during both AM and PM peak periods.

Based on a conversation with Richard Gamble of Clark County on 7/6/98, a background growth factor of 2 percent per year was assumed.





LEGEND

O - Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 7 FUTURE (1999) BASE

Table 4
Future (1999) Base Intersection Operation

	AM Pea	ak Hour	PM Pe	eak Hour
Intersection	Delay	LOS	Delay	LOS
NE JA Moore Road/NE 284 th Street	0.4	A/A	0.3	A/A
Bennet Road/61st Avenue/Site Access	2.0	A/A	1.5	A/A
NE Hyatt Road/NE Daybreak Road	1.6	A/A	0.6	A/A
NE 61 st Avenue/NE 82 nd Avenue	0.9	A/A	0.7	A/B

Unsignalized Intersection LOS:

A/A = Major street left turn LOS/minor street left turn LOS

Delay = Average vehicle delay in peak hour for entire intersection

Future (1999) Plus Project

This scenario represents conditions for full project operation. To estimate Future (1999) Plus Project traffic volumes, traffic generated by the project was added to the 1999 base volumes. The roadway network and geometries were assumed to remain the same as those for the existing case. Figures 8 and 9 show the Future (1999) Plus Project traffic volumes for the two alternatives.

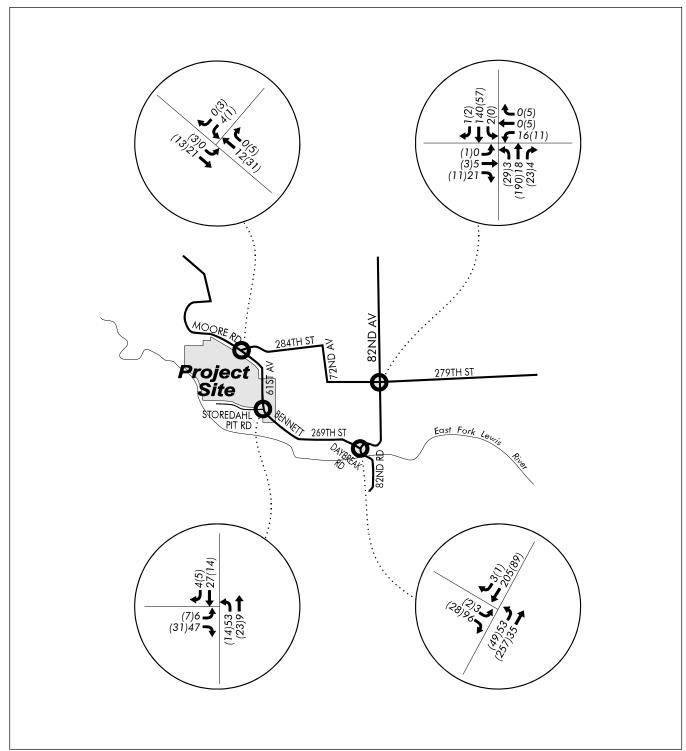
Table 5 shows the resulting levels of service for the four study intersections for this scenario. As the table shows, all four study intersections would operate at acceptable levels (LOS C or better) during both AM and PM peak periods.

SIGHT ACCESS/SIGHT DISTANCE

This section evaluates sight distance and stacking for each of the project access points along Bennet Road/61st Avenue. Sight distance evaluation was based on the guidelines set forth by the American Association of State Highway and Transportation Officials (AASHTO). As discussed earlier in this report, the 85th percentile speed along Bennet Road is approximately 50 miles per hour. Based on this speed, a minimum site distance of 500 feet is required along Bennet Road/61st Avenue¹¹.

A Policy on Geometric Design of Highways and Streets, American Association of State Highway and Transportation Officials, 1990, p. 762, Figure IX-40.





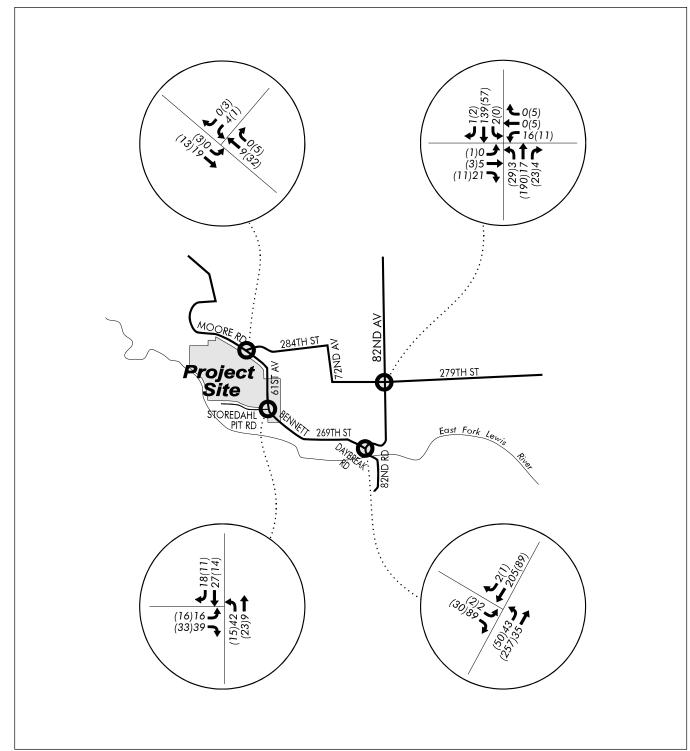
LEGEND

Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 8
FUTURE (1999) PLUS PROJECT
ALTERNATIVE 1 (Conveyor)





LEGEND

O - Study Intersection

AM(PM) - Peak Hour Traffic Volumes

Figure 9
FUTURE (1999) PLUS PROJECT
ALTERNATIVE 2 (Conveyor)

Table 5
Future (1999) Plus Project Intersection Operation

		AM Pea	k Hour	PM Pea	ak Hour
	Intersection	Delay	LOS	Delay	LOS
Alternative 1	NE JA Moore Road/NE 284 th Street	0.4	A/A	0.3	A/A
(conveyor)	Bennet Road/61st Avenue/Site Access	2.1	A/A	1.6	A/A
	NE Hyatt Road/NE Daybreak Road	1.7	A/A	0.6	A/A
	NE 82 nd Avenue/NE 279 th Street	0.9	A/A	0.7	A/B
Alternative 2	NE JA Moore Road/NE 284th Street	0.4	A/A	0.3	A/A
(no conveyor)	Bennet Road/61st Avenue/Site Access	2.0	A/A	1.8	A/A
	NE Hyatt Road/NE Daybreak Road	1.5	A/A	0.6	A/A
	NE 82 nd Avenue/NE 279 th Street	0.9	A/A	0.7	A/B

Unsignalized Intersection LOS:

A/A = Major street left turn LOS/minor street left turn LOS

Delay = Average vehicle delay in peak hour for entire intersection

Alternative 1

For Alternative 1, the only access point to the site would be Storedahl Pit Road (See Figure 1). At this location, sight distance is greater than the 500 feet minimum in both directions.

Based on the estimated number of vehicles entering and exiting the project site, less than one vehicle per minute would exit the project site driveway during the AM peak period. During the PM peak period, about one vehicle would exit the site every one and a half minutes. This would not generate significant queuing for vehicles exiting the project access.

Alternative 2

For this alternative, Storedahl Pit Road would remain the main access point. However, three additional access points would be utilized one at a time in order to truck the mined rock to the processing area. Figures showing the sight distance requirements for the four access points are shown in the appendix

of this report. As shown in the figures, two of these access points would be on the west side of 61st Avenue and one would be on the east side.

As with Alternative 1, the traffic volumes generated by this alternative would not generate significant queuing for vehicles exiting any of the project access points.

WEIGHT LIMITS

The proposed project would generate trips in the form of various vehicle types ranging from small private vehicles to large trucks. The trucks that would service the Daybreak Pit would meet the load requirements called out in WSDOT's "Permits For Oversized Overweight Vehicles" ¹².

Washington State Weight Table, section 46.44.041, per discussion with Virgle Barrett of J.L. Storedahl and Sons, March 19, 1996.

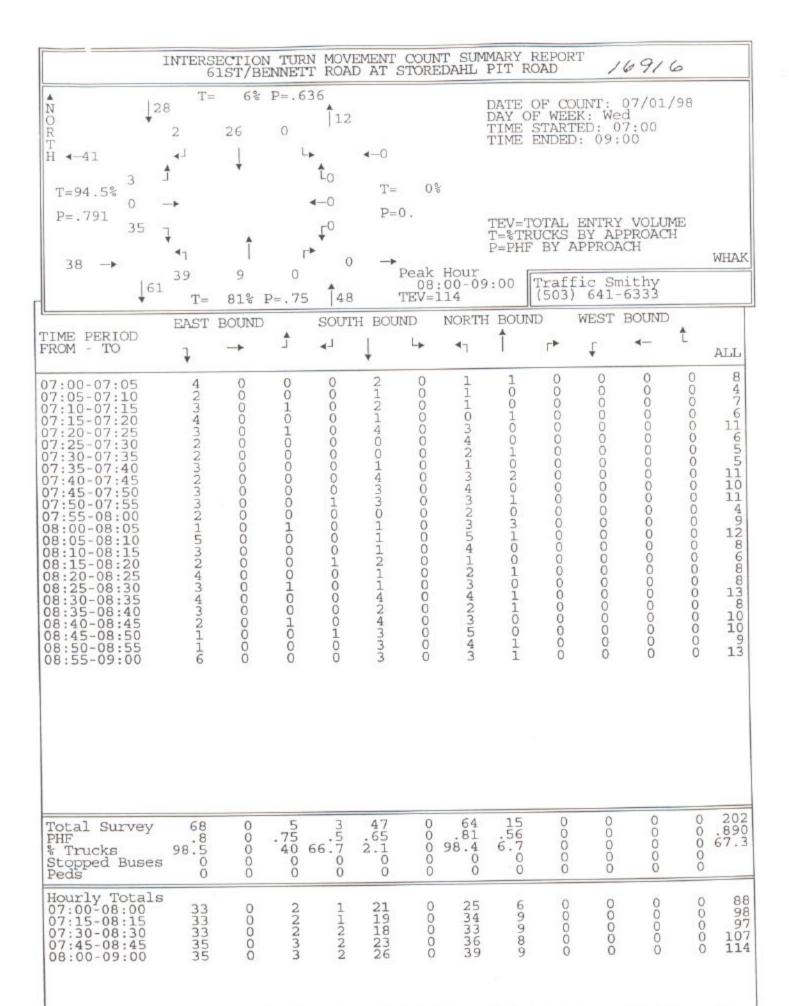
4. Mitigation

This section addresses the impacts associated with the proposed project and identifies possible measures to mitigate those impacts. In general, there are few traffic impacts created by the proposed project. Measures which can be undertaken to reduce the potential concerns regarding truck traffic would include the following:

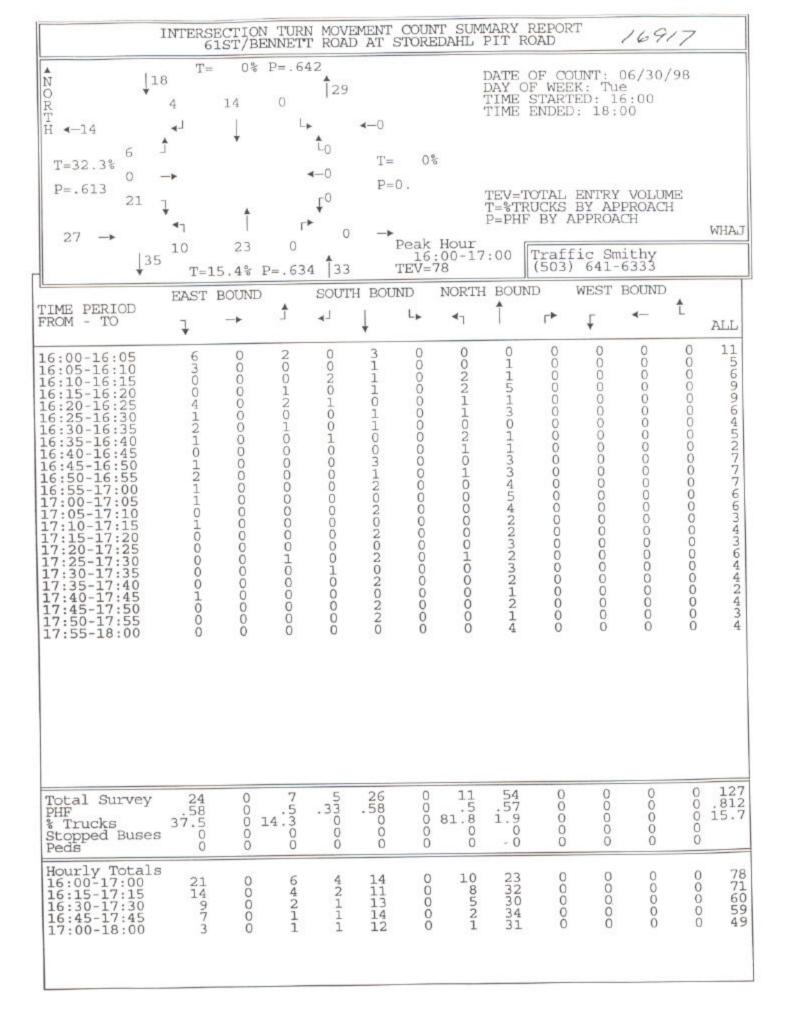
- Improved street lighting at site driveways to improve nighttime visibility in winter conditions;
- Work with school districts to identify school bus stop areas for children and provide widened shoulder areas (where needed or not already provided) on key routes in the area.

Appendix A

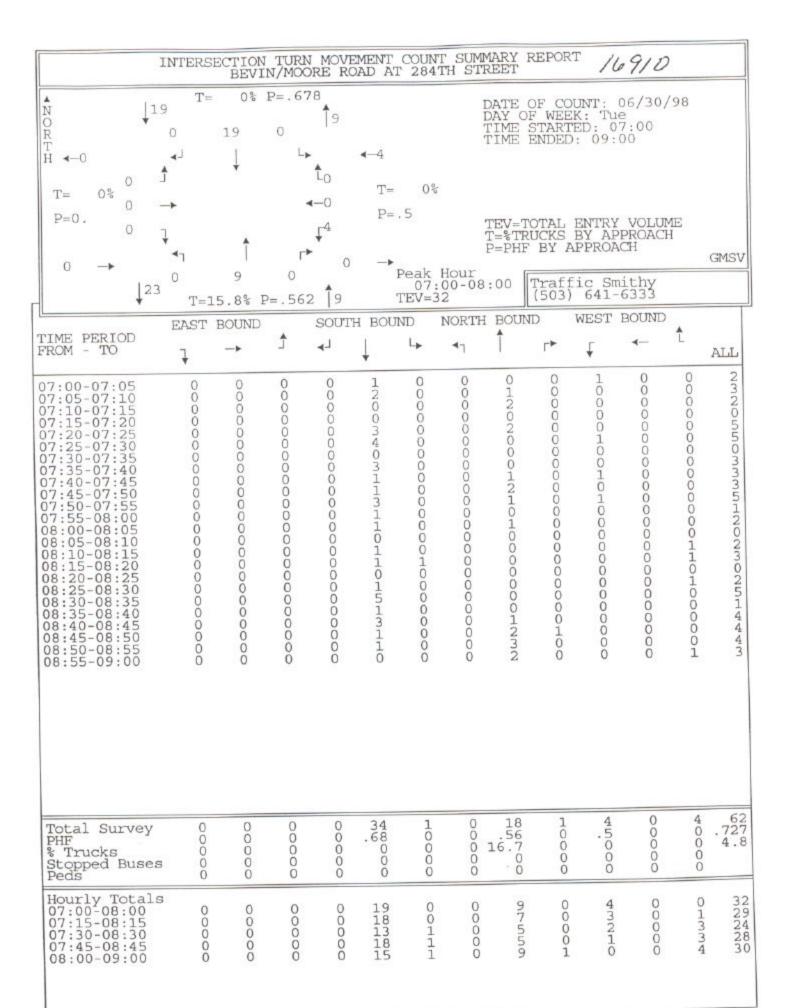
Traffic Counts



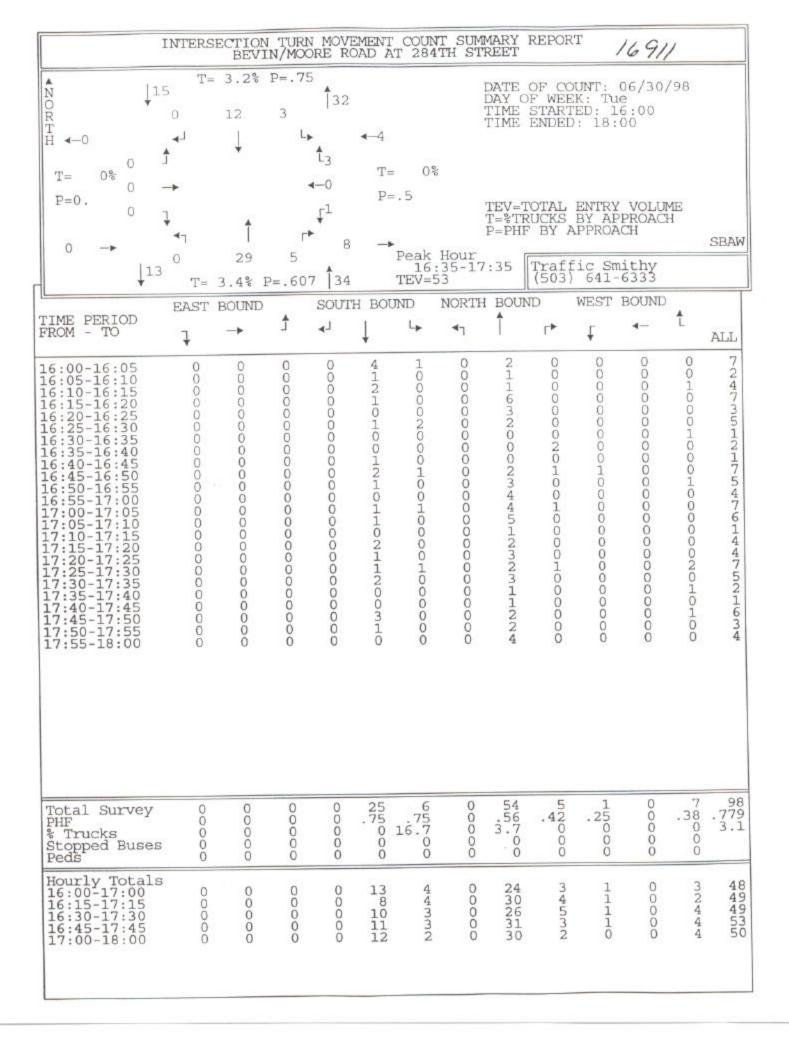
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08:00-08:15 0 0 0 0 0 0 0 0 08:15-08:30 0 0 1 1 1 08:30-08:45 0 0 0 0 0 0 0 0 0 08:45-09:00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10	0 12 0 6 0 9 0 12	4 1 2 2	0 0 0	0	0000	29 22 31 32
08:00-08:15 1 0 1 0 08:15-08:30 3 0 0 0 08:30-08:45 0 0 0 0 08:45-09:00 0 0 0 1 HEAVY TRUCKS (SEMI-TRACTOR TRAILE	000	0 0 0 0 0 0	0000	0 0 0 0 0 0	0	0 0 0	0 2 0 0
HEAVY TRUCKS (SEMI-TRACTOR TRAILE	0	0 3 0 0 0 0 0 3	0000	0 0	0	0000	5 3 1 4
08:00-08:15 8 0 0 0 08:15-08:30 6 0 0 08:30-08:45 9 0 0 08:45-09:00 8 0 0	0	0 9 0 6 0 9 0 8	0000	0 0	0 0	0000	17 12 18 16
BICYCLES 08:00-08:15	0	0 0 0	0000	0 0	0 0	0000	0000
PEDESTRIANSSOUTH	CROSSV WEST	WALK USE	AGE EAST		NORTH		ALL
08:00-08:15 0 08:15-08:30 0 08:30-08:45 0 08:45-09:00 0	0 0 0		0 0 0		NORTH 0 0 0 0		0000
Peak Hour by Movement PHF .97 0 .75 .5 % Trucks(all) 100 0 66.7 100 % Trucks(M+H) 100 0 33.3 50 Stopped Buses 0 0 0 0	3.8	0 .81 0 97.4 0 97.4 0 0	.56	0	0 0 0 0 0 0	0 0 0	.890 68.4 66.7
Hourly Totals 07:00-08:00 33 0 2 07:15-08:15 33 0 2 07:30-08:30 33 0 2 07:45-08:45 35 0 3 08:00-09:00 35 0 3	1 21 1 19 2 18 2 23 2 26	0 25 0 34 0 33 0 36 0 39	69989	0	0 0 0 0 0 0 0 0 0 0 0 0	0000	88 98 97 107 114



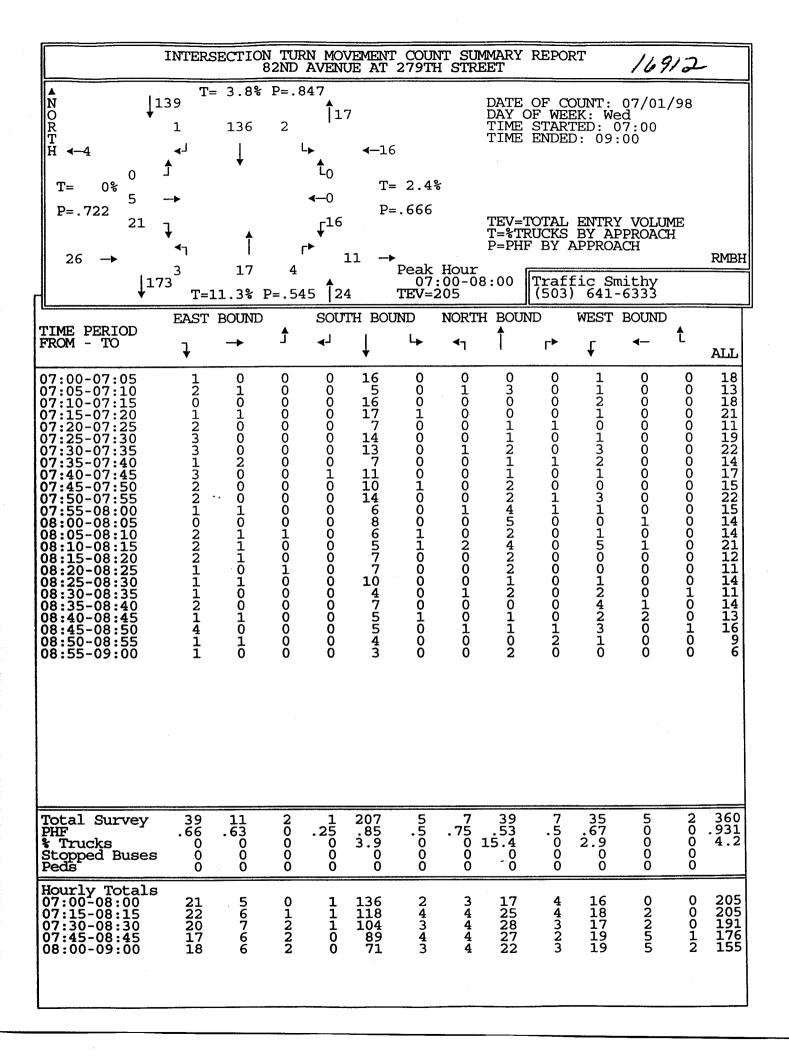
I	NTERSEC 61	TION ST/BE	TURN	MOVEM F ROAD	ENT (COUNT STOREI	PEAK DAHL	HOUR PIT R	REPO OAD	RT			
N	T= 8	0% 1 14	P= . 64	29	4 −0			DAY O	F WEE START	UNT: (K: Tue ED: 16 : 18:(6:00	98	
T= 37% 0 P=.613 21 27 → ↓35	J → ↓ ↓ 10 T=2'	23 7.3% P	0 0 0=.63	t ₀ √0 √0 0 4 133		0. Peak	Hour	T=%TR P=PHF	UCKS BY A	ENTRY BY AP PPROA		Æ I	UAHW
TIME PERIOD	8260000	BOUND	_	SOUT	H BOU	IND :	NORTH	BOUN	D	WEST	BOUND	4	
FROM - TO	1	-	J	47	1	L	4 7	1	Γ*	£	4-	5	ALL
ALL VEHICLES 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00	9 5 3 4	0 0 0	2 3 1 0	2 1 1 0	5 2 1 6	0 0 0	2 4 3 1	2 9 2 10	0000	0000	0000	0000	22 24 11 21
LIGHT TRUCKS 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00	(SINGLE 0 0 0 0	UNIT 0 0 0 0	2 AX 0 0 0 0	LES) 0 0 0	0 0 0	0 0 0 0	0 0 0	0 0 0	0000	0 0 0	0000	0 0 0	0 0 0
MEDIUM TRUCKS 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00	(SINGL 2 2 2 2 1	E UNIT	0 0 0	0 0 0 0 0	S) 0 0 0	0 0 0	1430	0000	0 0 0	0000	0 0 0	0000	3 6 5 1
HEAVY TRUCKS 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00	(SEMI-T	RACTOR 0 0 0 0	R TRA	0 0 0 0 0 0	0 0 0	0000	0 0 0 1	0000	0000	0 0 0	0000	0000	3 0 0 1
BICYCLES 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00	0 0 0 0	0 0 0	0 0 0	0 0 0	0 0 0 0	0 0 0	0000	0000	0000	0 0 0	0000	0000	0000
PEDESTRIANS 16:00-16:15 16:15-16:30 16:30-16:45 16:45-17:00		SOUTH 0 0 0 0			-CROS WEST 0 0 0	SSWAL	K USE	AGE EAST 0 0 0 0			NORTH 0 0 0 0		ALL 0 0 0 0
Peak Hour by PHF % Trucks(all) % Trucks(M+H) Stopped Buses	Movemer .58 42.9 42.9	0 0 1 0 1	.5 6.7 6.7	.5000	.58	0000	.63 90 90	.57	0000	0 0 0	0000	0000	.812 24.4 24.4
Hourly Totals 16:00-17:00 16:15-17:15 16:30-17:30 16:45-17:45 17:00-18:00	21 14 9 7 3	00000	64211	4 2 1 1	14 11 13 14 12	00000	10 8 5 2 1	23 32 30 34 31	00000	0000	0 0 0 0	0000	78 71 60 59 49



INTERSECTION TURN MOVEMENT COUNT PEAK HOUR REPORT BEVIN/MOORE ROAD AT 284TH STREET													
N O D D D D D D D D D D D D D D D D D D		0% I	0 L	78 19	4 −4			DAY O	F WEE	OUNT: CK: Tu ED: 0): 09:	7:00	98	
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TIME PERIOD FROM - TO		OUND -	Î	FOUTT	H BOU	IND L	NORTH	BOUN	r ≯	WEST	BOUND	t	ALL
ALL VEHICLES 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	0 0 0	0 0 0	0000	0	3 7 4 5	0000	0000	3 2 1 3	0000	1 1 1	0 0 0 0	0 0 0	7 10 6 9
LIGHT TRUCKS (07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	SINGLE 0 0 0 0	UNIT 0 0 0	2 AX 0 0 0 0	LES) 0 0 0	0000	0 0 0	0 0 0 0	0000	0 0 0	0000	0 0 0	0000	0000
MEDIUM TRUCKS 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	(SINGLE 0 0 0 0	UNIT 0 0 0 0	, 2 0000	AXLE 0 0 0 0	S) 0 0 0	0000	0000	0 0 0	0000	0 0 0 0	0000	0 0 0	0 0 0 0
HEAVY TRUCKS (07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	SEMI-TI 0 0 0 0	RACTOR 0 0 0 0	TRA 0 0 0 0	O 0 0 0 0 0	0000	0 0 0	0000	0000	0000	0000	0 0 0	0000	0000
BICYCLES 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	0 0 0	0 0 0	0 0 0	0000	0000	0000	0 0 0	0000	0 0 0	0 0 0	0000	0000	0 0 0
PEDESTRIANS 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00		SOUTH 0 0 0			-CROS WEST 0 0 0	SSWAL	K USE	AGE EAST 0 0 0 0			NORTH 0 0 0 0		ALL 0 0 0 0
Peak Hour by PHF % Trucks(all) % Trucks(M+H) Stopped Buses	Movemen 0 0 0 0	t 0000	0000	0000	.68	0 0 0	0 0 0	.75 0 0	0000	1 0 0 0	0 0 0 0	0000	.8
Hourly Totals 07:00-08:00 07:15-08:15 07:30-08:30 07:45-08:45 08:00-09:00	0000	00000	00000	0 0 0 0	19 18 13 18 15	0 0 1 1 1	00000	97559	0 0 0 0 1	43210	00000	0 1 3 3 4	32 29 24 28 30



I	NTERSE	CTION BEV	TURN IN/MO	MOVEN ORE RO	ENT DAD A	COUNT T 284	PEAK TH ST	HOUR REET	REPO	ORT			
N ↓1 O R T H ←0	T= 4 0 ↑	0% 11 ↓	P=.7	†35 ►	4 –5			DAY C	F WEI	OUNT: EK: Tu TED: 1 D: 18:	6:00	98	
T= 0% 0 P=0. 0 0 →	→ 1 0 T=	31	7 3 P=.77	4-0 ↓1 6 2 134	T= P= →	.625 Peak	45-17	T=%TF P=PHF	Traf	ENTRY BY AF APPROA	nithv	iE I	SBAW
	-	BOUND		SOUT	H BOU	11000		BOUI			BOUND	20	
TIME PERIOD FROM - TO	Į	-	Î	ل◄		L	4 7	1	┌►	t	4 −	Ĺ	ALL
ALL VEHICLES 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45	0000	0 0 0	0 0 0	0 0 0	3 2 4 2	1 1 0	0000	9 10 7 5	1 1 1 0	1 0 0 0	0000	1 0 2 1	16 14 15 8
LIGHT TRUCKS 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45	SINGLE 0 0 0 0	UNIT 0 0 0 0	2 AX 0 0 0 0	LES) 0 0 0 0	0000	0 0 0	0000	0 1 0 0	0 0 0	0000	0000	0 0 0	0 1 0 0
MEDIUM TRUCKS 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45	(SING) 0 0 0 0	LE UNI 0 0 0 0	T > 2	AXLE 0 0 0 0	S) 0 0 0	0000	0 0 0	0000	0000	0 0 0	0000	0000	0 0 0
HEAVY TRUCKS 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45	(SEMI- 0 0 0 0	TRACTO 0 0 0 0	R TRA 0 0 0 0	ATLER) 0 0 0 0	0000	0 0 0	0000	0 0 0	0 0 0	0 0 0	0000	0 0 0 0	0000
BICYCLES 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45	0000	0 0 0	0000	0 0 0	0 0 0	0000	0 0 0	0 0 0	0000	0000	0 0 0	0 0 0	0000
PEDESTRIANS 16:45-17:00 17:00-17:15 17:15-17:30 17:30-17:45		SOUTH 0 0 0 0			-CRO WEST 0 0 0	SSWALF	(USE	AGE EAST 0 0 0 0			NORTH 0 0 0 0	-,	ALL 0 0 0
Peak Hour by PHF % Trucks(all) % Trucks(M+H) Stopped Buses	0	nt 0 0 0 0 0	0000	0 0 0	.69	.75	0000	.77 3.2 0 0	.75	.25	0 0 0	.5000	.828 1.9 0
Hourly Totals 16:00-17:00 16:15-17:15 16:30-17:30 16:45-17:45 17:00-18:00	00000	0 0 0 0	00000	0	13 8 10 11 12	44332	00000	24 30 26 31 30	3 4 5 3 2	1 1 1 0	00000	3 2 4 4 4	48 49 49 53 50



II	VTERSEC	TION '	TURN 2ND <i>I</i>	MOVEN	ENT E AT	COUNT 279TH	PEAK STRE	HOUR ET	REPO	RT			
N	T= 39 1 ↓	4.3%			4 −16			DATE DAY C	OF CO F WEE START ENDED	K: We ED: 0	7:00	/98	
T= 0% 5 P=.722 21 -	∱ → ↓ ∢ ₇ 3	† 17	دا 4	t ₀ ←0 ↓16	P=	6.3% 6.666 Peak	Hour	T=%TF P=PHF	UCKS BY A	BY AP APPROA		ME H	RMBH
↓17	ว −	0.8% P			H BOU	TEV=2		B:00 BOUN		641-6	BOUND		
rime period from - To	Ţ	→	.	↓	 	پ	4 7	T .	Γ►	t	4	L 	ALL
ALL VEHICLES 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	3 6 7 5	1 1 2 1	0 0 0	0 0 1 0	37 38 31 30	0 1 0 1	1 0 1 1	3 2 4 8	0 1 1 2	4 2 6 4	0000	0 0 0	49 51 53 52
LIGHT TRUCKS (07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	SINGLE 0 0 0 0	UNIT 0 0 0 0	2 AX 0 0 0 0	LES) 0 0 0 0	0 0 1 2	0 0 0 0	0 0 0 0	0 0 0 1	0 0 0 0	0 0 0	0 0 0	0 0 0	0 0 1 3
MEDIUM TRUCKS 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	(SINGL 0 0 0 0	E UNIT	C > 2 0 0 0	AXLE 0 0 0 0	S) 0 0 0 2	0 0 0 0	0 0 0	0 0 2 0	0 0 0	0 1 0 0	0 0 0	0 0 0	0 1 2 2
HEAVY TRUCKS 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	(SEMI-T 0 0 0 0 0	RACTO I 0 0 0 0	R TRA 0 0 0 0	O 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 1	0 0 0	0 0 0	0 1 0 1	0 0 0	0 0 0	0 0 0	0 0 0	0 1 0 2
BICYCLES 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
PEDESTRIANS 07:00-07:15 07:15-07:30 07:30-07:45 07:45-08:00		SOUTH 0 0 0 0			CRO WEST 0 0 0 0	SSWAL	K USE	AGE EAST 0 0 0 0			NORTH 0 0 0 0	I	ALL 0 0 0
Peak Hour by PHF % Trucks(all) % Trucks(M+H) Stopped Buses	Movemer . 75 0 0 0	.63 0 0	0000	.25	.89 4.4 2.2 0	.5	.75 0 0 0	.53 29.4 23.5 0	.5	.67 6.3 6.3	0 0 0	0000	.966 5.9 3.9
Hourly Totals 07:00-08:00 07:15-08:15 07:30-08:30 07:45-08:45 08:00-09:00	21 22 20 17 18	5 6 7 6	0 1 2 2 2	1 1 0 0	136 118 104 89 71	2 4 3 4 3	3 4 4 4 4	17 25 28 27 22	4 4 3 2 3	16 18 17 19 19	0 2 2 5 5	0 0 0 1 2	205 205 191 176 155

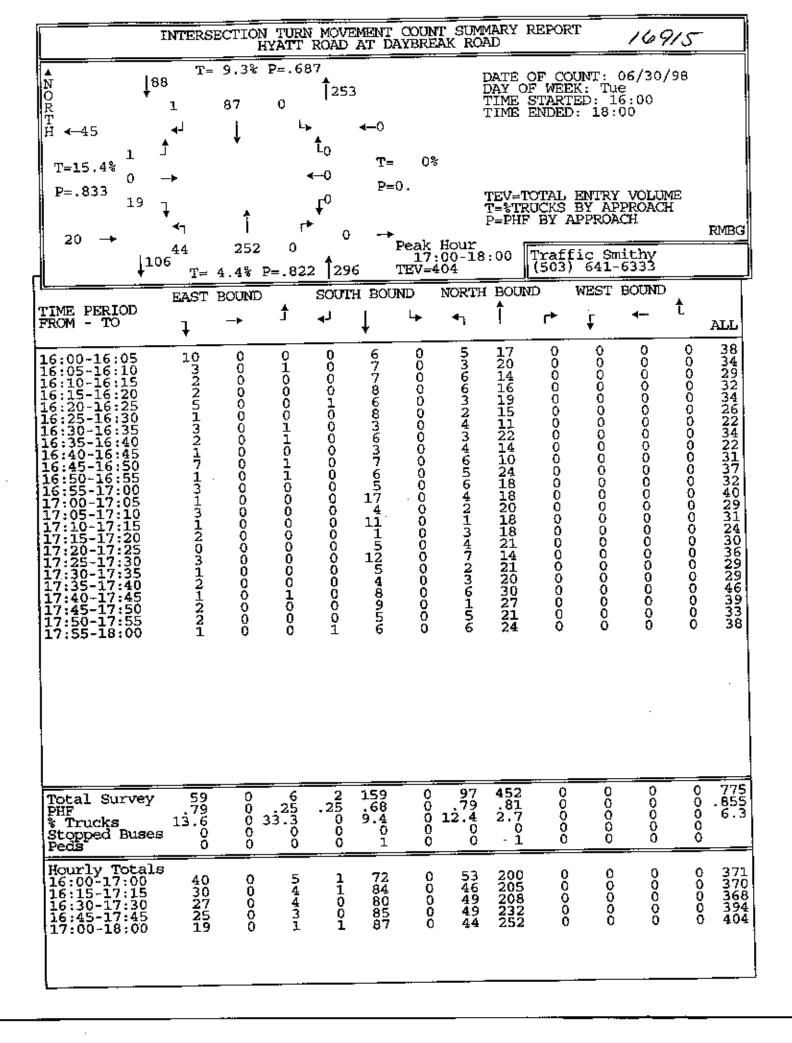
	NTERSE	CTION 82	TURN ND A	MOVENUE	ENT AT 2	COUN 79TH	T SUM STRE	MARY ET	REPOR'	r	16;	9/3	
N	T=	7.8% F	°=.80 0 ↓	5 191	←21 T=	0% . 52 5		DATE DAY O		UNT: K: We	07/01/ d 6:00 00	98	
P=.625 11 ↓ 15 →	ชีว 28 ช- ว	185 :.3% P:	r► 23 =.830	↓ ¹¹ 26 1236	→ ,	Peak	Hour 00-18	P=PHF	OTAL UCKS BY A Traff (503)	PPROA		E I	RMBI
TIME PERIOD ROM - TO	EAST E			SOUTH	BOUI	ND L	NORTH	BOUN	i⊅ 1D	west f	BOUND	î	ALL
16:00-16:05 16:05-16:10 16:10-16:15 16:15-16:20 16:20-16:35 16:25-16:30 16:35-16:40 16:40-16:45 16:45-16:55 17:05-17:00 17:05-17:15 17:15-17:20 17:15-17:30 17:25-17:30 17:30-17:45 17:45-17:50 17:55-18:00	101260000100002110210022	202000004111010000002000	0000000010100000000001000	000000000000000000000000000000000000000	324474213432725565154394	101100000000000000000000000000000000000	112013134312234322122223	84 1092977 11254071415186816	1222303210000211333713213	011101020102102010122200	0230000012000100001300	0002110011100030011000000	17 1200007 130007 112321 13232 113232 113232 1232 12322 1232 12322 12322 12322 12322 12322 12322 12322 12322 12322 12322 12322 12322 1232
Total Survey PHF % Trucks Stopped Buses Peds	22 .69 4.5 0	14 .38 0 0	.25 00 0	25 0 0 0	95 .88 7.4 0	3 0 33.3 0 0	50 .7 2 0	311 .78 2.3 0	39 .64 2.6 0 0	20 ,46 0 0	13 .31 0 0	.42 .42 0 0	586 .850 3.1
Hourly Totals 16:00-17:00 16:15-17:15 16:30-17:30 16:45-17:45 17:00-18:00	11 11 5 8 11	11 8 8 6 3	2 2 2 1	2 2 2 2 2	39 44 45 49 56	3 1 0 0	22 27 30 27 28	126 163 175 179 185	16 14 16 17 23	10 9 12 11	8 4 4 5 5	7 8 8 6 5	256 294 304 313 330
<u> </u>													

		= = -				<u></u>			·······					
_ _		NTERS	ECTION	TUR 82NE	N MO	/EMENT VUE AT	COUN 2791	T PE	AK HOU REET	JR REI	PORT			
A N O R T H 4 –35	ţs	2 4	= 1.7% 56 ↓	P=.		±91, 4 –2	!1	ë.	DAY TIME	OF WI	SEK: V STED:	16:00	•	
T= 0% P=.625	1 3 11	.ı → ↓ •••	†		¹ 5 4–5 ¹¹	P	'= 0 '=.75	1 %	T = 3.1	TOTAL RUCKS IF BY	BY A	RY VOLI APPROA DACH	UME CH	
	↓ 78	28 T ≃	185 2.1%	2 P=.8	3 ▲	26 – 36		Hour :00-1	L8:00	Traf	fic 8	mithy	<u>"</u>	RMB1
<u> </u>			BOUND			TH BO		<u> </u>	TH BOU			BOUN		
FIME PERIO	D ———	7	→	ŧ	47	1	L _b	* 1	1	r•z	t weel	- BOUNI	t	ALL
ALL VEHICL 17:00-17:1 17:15-17:3 17:30-17:4 17:45-18:0	5 0 5	2 2 3 4	1 0 2 0	0 0 1 0	2000	14 16 10 16	0000	9 7 5 7	59 42 44 40	3 7 7 6	3 1 5 2	1 0 1 3	3200	97 77 78 78
GIGHT TRUC L7:00-17:1 L7:15-17:3 L7:30-17:4 L7:45-18:0	5 `	SINGLE 0 0 0 0	UNIT 0 0 0 0	2 A) 0 0 0 0	KLES) 0 0 0 0	0 1 0 0	0000	0 1 0 0	0 0 1 0	0 1 0 0	0000	0000	0000	0 3 1
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7:00-17:15 7:15-17:30 7:30-17:45 7:45-18:00			SOUTH 0 0 0 0			-CROS WEST 0 0 0	SSWALF	(USE	AGE EAST 0 0 0 0			NORTH 0 0 0 0	:	ALL 0 0 0
eak Hour h HF Trucks(al Trucks(M- topped Bus	ll) H) Bes	0 0 0 0 0	.38 . 0 0	25 0 0	.25 0 0	.88 1.8 0 0	000	.78 3.6 0	.78 1.6 1.1	.82 4.3 0	.55 0 0	.42	.42	.850 1.8 .6
ourly Tota 6:00-17:00 6:15-17:15 6:30-17:30 6:45-17:45 7:00-18:00	ls)	11 11 5 8 11	11 8 6 3	22221	22222	39 44 45 49 56	3 1 0 0	22 27 30 27 28	126 163 175 179 185	16 14 16 17 23	10 12 12	8 4 4 5 5	7 8 8 6 5	256 294 304 313 330

<u> </u>	INTERSE	CTION H	TURN YATT	MOVI ROAD	MENT AT D	COUN AYBRE	T SUM AK RO	MARY AD	REPOR'	r	169	14	
N ↓2 O ↓2 R T T + 4-41	T= 203 2 ·	4.1% 201	P= . 84 0 L,		← 0			DAY C TIME	OF CO F WEE START ENDED	K: Tw ED: 0	7:00	'98	
T=55.4% 0 P=.787 83 85 →	Î →► ↓ 41 39 84 T-4:	34 8.8% F	ر ، 0	10 ←0 ↓0 0 173		0. Peak	Hour :00-08	T=%TF P=PHE	OTAL RUCKS BY A Traff (503)	BY AP PPROA		Æ H	RMBF
	EAST				H BOU			I BOUN	L. <u></u>		BOUND	_	
rime period From - To	7	→	Ţ	ل≱		L _F	4 7	Ī	r*	ţ	-	L	ALL
07:00-07:05 07:05-07:15 07:10-07:15 07:15-07:20 07:20-07:25 07:25-07:30 07:35-07:40 07:35-07:40 07:45-07:50 07:45-07:50 07:55-08:05 08:05-08:15 08:15-08:25 08:25-08:30 08:35-08:35 08:35-08:45 08:45-09:00 08:55-09:00	876360706325145462165566	000000000000000000000000000000000000000	010000001000000001001000	00110000000000000000000	2237702148 21122148 211221112111988445 211560	000000000000000000000000000000000000000	323735126430023153387876	012341702284702252243214	0000000000000000000000	0000000000000000000000	000000000000000000000	00000000000000000000000000	334994403369433227795422107006 322333333223323222322222222222222222
Total Survey PHF % Trucks Stopped Buse Peds	56.3	00000	4 25 25 0	.25 .50 0 0	314 .87 3.8 0 0	00000	102 .65 76.5 0	68 .61 7.4 0 .0	00000	00000	00000	00000	634 .911 28.1
Hourly Total 07:00-08:00 07:15-08:15 07:30-08:30 07:45-08:45 08:00-09:00	83 72 65 64 61	0000	21232	2 1 0 0	201 183 158 129 113	0000	39 46 40 49 63	34 40 41 41 34	000000000000000000000000000000000000000	0000	0 0 0 0	0000	361 343 306 286 273

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			NTERSE	H	YATT	ROAD	AT D	AYBRE	AK RO	AD					
ANORTH ←	41		T=	3.9% 201	P=.8	90 36	4-0			DAY O TIME	F WEE START	OUNT: K: Tu ED: 0	7:00	98	
T=5	-41 50.6% 923	2 0 83	. →	+		t ₀ t ₀	Т=	: 0% :0.	ī	TEV=T	OTAL	ENTRY	VOLUM PROACI	Æ	
85	5 → •	↓ 28	*	ौ 34 3.8% F	0 9=.79	0	→	Peak 07: TEV=3	80-00	P=PHF	BY	PPROA	CH		RMBF
<u></u>		<u></u>	EAST	BOUND		SOUT	H BOU	IND	NORTI	I BOUN	ID G	WEST	BOUND		
TIME FROM	PERI - TO	OD	Ţ	→		√J	ļ	Ļ	4 1	Î	Γ *	<u> </u>	4 −	T.	ALL
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07:0007:1007:1007:3	T TRU 0-07: 5-07: 0-07: 5-08:	15 30 45	(SINGLE 0 1 0 0	UNIT 0 0 0 0	2 AX 0 0 0 0	(LES) 0 0 0 0	0 0 1 1	0000	0000	0 0 0 2	0	0 0 0	0	000	0113
07:0 07:1 07:3	UM TR 0-07: 5-07: 0-07: 5-08:	15 30 45 00	(SINGI 0 1 2 0	000	0 0 0	AXLE 0 0 0	(S) 1 3 0 0	000	1 2 0 0	0 0 0 1	0000	0	0 0 0	0000	3622
07:0 07:1 07:3	Y TRU 0-07: 5-07: 0-07: 5-08:	15 30 45	(SEMI-1 12 7 11 8	RACIO 0 0 0 0	0 0 0 0	AILER) 0 0 0 0	0 0 1 0	0 0 0 0	10 5 5	0000	0000	000	0 0 0	0	18 17 17 13
07:0 07:1 07:3	CLES 0-07 5-07 0-07 5-08	:45	0	0 0 0	0	0000	0 0 0	0000	0	0 0 0 0	0	0 0 0	0000	000	0000
07:0 07:1	STRIA 00-07 15-07 30-07 15-08	:15		SOUTH 0 0 0 0			-CRO WEST 0 0	SSWAL	K USE	AGE EAST 0 0 0			NORTH 0 0 0 0 0	I	ALT. 0
PHF % Tr % Tr Stor	rucks rucks oped	(all) (M+H) Buses		nt 0 0 0	.50 50 50	50 50 50	.88 3.5 2.5 0	0000	74.4 74.4 0	.61 8.8 2.9 0	0 0 0	0	0	000	.920 23 21.6
10/24	rly T 00-08 15-08 30-08 45-08 00-09	otals :00 :15 :30 :45 :00	83 72 65 64 61	00000	2 1 2 3 2	2 1 0 0	201 183 158 129 113	0000	39 46 40 49 63	34 40 41 41 34	0000	0000	00000	0000	361 343 306 286 273
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I	NTERSEC	TION H	TURN IYATT	MOVE ROAD	MENT AT D	COUNT AYBRE	PEAK AK RO	HOUR AD	REPO	RT			
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20 → ↓10	06 T=	252 1% I	0 P=.88	0 0 † 29		Peak 17: TEV=4	00 - 18	:00	(503)	ic Sm 641-6	333		
TIME PERIOD FROM - TO	EAST	BOUND →	ţ	SOUTI √J	H BOU	NTD -	NORTE	BOUN	D r*	WEST	BOUND 4—	t	ALL
ALL VEHICLES 17:00-17:15 17:15-17:30 17:30-17:45 17:45-18:00	5545	0000	0	0 0 0	32 18 17 20	0000	7 14 11 12	56 53 71 72	0000	0000	0000	0000	100 90 104 110
LIGHT TRUCKS 17:00-17:15 17:15-17:30 17:30-17:45 17:45-18:00	(SINGLE 0 0 0 0 0	UNIT 0 0 0 0	2 AX 0 0 0 0	LES) 0 0 0	2000	0000	0	000	0000	0	0000	0000	3 1 0 0
MEDIUM TRUCKS 17:00-17:15 17:15-17:30 17:30-17:45 17:45-18:00	(SINGL 0 0 0 0	E UNI' O O O	T > 2 0 0 0	AXLI 0 0 0 0	3S) 0 0 2 4	0000	0000	0000	0	0000	0	0000	0 0 2 4
HEAVY TRUCKS 17:00-17:15 17:15-17:30 17:30-17:45 17:45-18:00	(SEMI-T 0 0 0 0	RACIO 0 0 0 0	R TRA	AILER 0 0 0 0) 0 0 0	0000	0 0 0	1000	0	0	0000	0000	1 0 1
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PEDESTRIANS 17:00-17:15 17:15-17:30 17:30-17:45 17:45-18:00		SOUTH	[-CRO WEST 0 0 0 1	SSWAL	K USE	AGE- EAST 0 0 0 1			NORTH 0 0 0 0	_ [ALL 0 0 0 2
Peak Hour by PHF % Trucks(all) % Trucks(M+H) Stopped Buses	Movemen .95 0 0	nt 0 0 0	.25 0 0	.25 0 0	10.3 8 0	0000	.79 2.3 0	.88 .8 .4	0	0000	0000	0000	.918 3 2
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TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229 (503) 641-6333 FAX (503) 643-8866

*** Special Speed Study (#203) ***

Data Starts : 16:00 on 06/29/98

Site ID : 1BEN49 Data Ends : 08:00 on 07/01/98 Info 1 : BENNET ROAD

Adj. Factor: 1.000%

Info 2 : S OF STROEDAHL *****************

Cane #1 Info : NORTHBOUND : AXLE, SPEED Modes

Sensor Spacing: 16.0' : Axle-Axle

Sensors

************************ Lane 1 Special Speed Study ******************

		#1	#2	#3	#4	#5	#6	#7	₽.В.	#2	# 11.11	MTT	##						
		0-	20-	25-	30-	35-	40-	45-	50-	\$ 5-	60-	65-	70-	75-	80-	85-			
Date	Time	19.9	24.9	29.9	34.9	39.9		49.9	54.9	59. 9	64.9	69.9	74.9	79.9	84.9	89.9	Other	Error	Total
06/29/98	16:00	0	1	1	1	9	16	12	В	2	a	0	0	0	0	0	0	ó	50
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	18:00	1	ō.	0	0.	. 2	3	13	11	9	2	0	0	0	0	Ů	0	0	41
	19:00	Ò	0	0	0	1	2	6	7	4	0	Q	0	0	٥	0	O-	0	22
	20:00	0	0	0	2	4	6	8	4	1	1	0	0	0	0	a	0	0	. 26
	23:00	C	0	0	0	4	9	4	3	o	Ö	¢	D	0	0	0	0	Q	20
	22:00	0	0	0	0	0	1	1	1	1	0	Q	Q	đ	o	0	0	0	4
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10% Speed: 37.5mph Avg Speed: 47.2mph

50% Speed: 47.6mph

85% Speed: 53.7mph

Page: 1

7/01/98 .0:11:09

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229 (503) 641-6333 FAX (503) 643-8866

Page: 2 Bennet Road S. y Storedan1

					1	(503) 64	1-63	333	FAX	(5	03}	643	-886	6	- 7		NY	3
***	***	***	***	***	***	***	Lane	1 :	Spec	ial	Spe	ed S	Stud	y **	***	***	***	NY ****	***
		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	#14	#15	#16		
		D-	20-	25-	30-	35-	40-	45-	50-	55-	60-	65-	70-	75-	80-	85-			
Date	Time	19.9	24.9	29.9	34.9	39.9	44.9	49.9	54.9	59.9	66.9	69.9	74.9	79.9	84.9	89.9	Other	Error 7	Cotal
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lueve	ge Hour			, () E	. 9	9 5	4	. 3	1	L C) (0 1	• (; ; 51.10		30

10% Speed: 32.3mph

Avg Speed: 41.6mph

50% Speed: 39.7mph

85% Speed: 51.1mph

)7/01/98 \0:11:09

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229

(503) 641-6333 FAX (503) 643-8866

Page: 3 Bennet-Road S. of Store dahl

						(503) 64	11-6	333	FA	K (5	03)	643	-886	6			1	'B
****	***	****	***	***	***	***	Lane	1	Spec	ial	Spe	ed S	Stud	y **	***	***	***	***	k * * * * *
		#1	#2	#3	#4	#5	#6	#7	#8	#9	#10	#11	#12	#13	#14	#15	#16		
		0-	20-	25-	30-	35-	40-	45-	50-	55-	60-	65-	70-	75-	80-	85-			
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	2:00	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	1
	3:00	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	1
	24:00	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	5:00	0	0	0	0	0	4	2	1	0	0	0	0	0	0	0	0	0	7
	06:00	0	0	0	0	7	10	4	4	1	0	0	0	0	0	0	0	0	26
	7:00	0	0	1	15	15	2	3	0	1	0	0	0	0	0	0	0	0	37
ily Tota	1 #1		0	2	15	22	17	10	8	4	0	0	0	0	0	0	0	0	78
-	rcent	0%	0%		19%	28%	22*	134	10%	5*	0*	0*	01	0%	01	0*	0%	0*	
Cum. Per		0%	0%			50%	71%	84%	94%	100%									
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arczage		_		-			- Cnee	4. 22	emmh.		ins en	ed: 31	1 mmh		85%	Speed:	47.8m	oh.	

17/01/98 LO:11:09

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229 (503) 641-6333 FAX (503) 643-8866

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NB

Special Speed Study Final Report *********** Data Starts: 16:00 on 06/29/98 Site ID: 1BEN49 Data Ends : 08:00 on 07/01/98 Info 1 : BENNET ROAD Adj. Factor: 1.000% Info 2 : S OF STROEDAHL **************** #12 65-70-75-80-60-25-45-50-55-30-35-20-84.9 89.9 Other Error Total 69.9 74.9 64.9 49.9 54.9 59.9 19.9 24.9 29.9 34.9 39.9 44.9

0 . 1014 0 3 0 0 0 190 167 138 63 11 151 272 0% 0% 0% 0% 19% 14% 6% 14 0% 15% 21 Percent 01 0% 98% 99% 100% 92% 624 78% 16% 43% Cum. Percent 25 0 1 0 0 6 0 0 0 85% Speed: 52.3mph 50% Speed: 41.9mph 10% Speed: 32.7mph Avg Speed: 42.7mph ADT: 1690

Page: 1

7/01/98 0:11:22

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229

(503) 641-6333 FAX (503) 643-8866

*** Special Speed Study (#203) ***

********** Data Starts: 16:15 on 06/29/98

3ite ID : 1BEN47 Data Ends : 08:00 on 07/01/98 Info 1 : BENNET ROAD

Adj. Factor : 1.000% Info 2 : S OF STOREDAHL *************************

: SOUTHBOUND Lane #1 Info : AXLE, SPEED Modes

Avg Speed: 44.6mph

Sensor Spacing: 16.0' **************** : Axle-Axle

		#1 0- 19.9	#2 20- 24.9	#3 25- 29.9	#4 30- 34.9	#5 35- 39.9	#6 40- 44.9	#7 45- 49.9	#8 50- 54.9	#9 55- 59-9	#10 60- 64.9	#11 65- 69.9	#12 70- 74 ,9	#13 75- 79.9	#14 80- 84.9	85- 89.9	Other	Error	Total
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	19:00	0	2	1	0	. 2	5	4	3	2			0	0	0	0	9	0	15
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)7/01/98 .0:11:22

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229 (503) 641-6333 FAX (503) 643-8866

Page: 2 Bennet Rd. South of Storeduhl

#10 #13 #12 #13 #14 #15 #16

		#1	#2	#3	#4	45	#6	#7	#\$	#9	#10	#13	#12	#13	#14	#15	#10		
		0-	20-	25-	30-	35-	40-	45-	50-	65-	60-	6 5-	70-	75-	BÓ-	85-			
Date	Time	19.9	24.9	29.9	34.9	39.9	44.9	49.9	54.9	59.9	64.9	69.9	74.9	79.9	84.9	89.9	Other	Error	Total
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7/01/98 0:11:22

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

Page: 3 Bennet Road South of Storedahl

PORTLAND, OREGON 97229 (503) 641-6333 FAX (503) 643-8866

					,	(503) 64	1-6	333	PAZ	((5	031	643	-000	.6				S &	3
****	****	***	***	***	***	***	Lane	1	Spec	ial	Spe	ed s	Stud	У **	***	****	****	***	*****	
		#1	#2	#3	#1	#5	#6	#7	#8	#9	#10	[11	#12	#13	#14	#15	#16			
		0-	20-	25-	30-	35-	40-	45-	50-	55-	60-	65-	70-	75-	80-	85-				
Date	Time	19,9	24.9	29.9	34.9	39.9	44.9	49.9	54.9	59.9	64.9	69.9	74.9	79.9	84.9	89.9	Other	Error	Total	
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		Asso 5	Speed:	39.1m	oh.	101	Speed	1: 22.	7mph		501 Sp	eed: 4	2.5mph		B54 .	Speed:	48.2mg	ah.		

)7/01/98 LO:11:22

ADT: 1525

TRAFFIC SMITHY 1225 NW MURRAY BLVD SUITE 111

PORTLAND, OREGON 97229

(503) 641-6333 FAX (503) 643-8866

SB

85% Speed: 49.1mph

Page: 4

Special Speed Study rinal Report

10% Speed: 25.8mph

Avg Speed: 37.8mph

Site ID : 1BEN47 Data Starts : 16:15 on 06/29/98

Info 1 : BENNET ROAD Data Ends : 08:00 on 07/01/98

50% Speed: 37.3mph

Info 2 : S OF STOREDAHL Adj. Factor : 1.000%

Date	Time	#1 0- 19.9		25-	30-	35-	40-	45-	50-		60-	65-	70-	75-	-02	85-		Brror	Total
Grand To	otal #1 Percent			210 224													\$0	o ok	939
Cum. I	Percent re Hour	01	71	29%	464	554	681	661	974	991	100%								24

Appendix B

Level of Service Descriptions

UNSIGNALIZED INTERSECTIONS (Two-Way Stop Controlled)

Unsignalized intersection level of service is reported for the major street and minor street (generally, left turn movements). The method assesses available and critical gaps in the traffic stream which make it possible for side street traffic to enter the main street flow. The 1994 Highway Capacity Manual describes the detailed methodology. It is not unusual for an intersection to experience level of service E or F conditions for the minor street left turn movement. It should be understood that, often, a poor level of service is experienced by only a few vehicles and the intersection as a whole operates acceptably.

Unsignalized intersection levels of service are described in the following table.

Unsignalized In	ntersections	Avg Total Delay
Level of Service	Expected Delay	(Sec/Veh)
A	Little or no delay	<u><</u> 5.0
В	Short traffic delay	5.1-10.0
С	Average traffic delays	10.1-20.0
D	Long traffic delays	20.1-30.0
E	Very long traffic delays	30,1-45,0
F	Extreme delays potentially affecting other traffic movements in the intersection	> 45

Source: Highway Capacity Manual, Special Report 209 (Third Edition), Transportation Research Board Washington, D.C., 1994.

Appendix C

Level of Service Calculations

METAN . CHD

AM Peak Hour Impact Analysis Report Level Of Service

intersection	Base Del/ V/	Future Del/ V/	Change in
	LOS Veh C	LOS Veh C	
2 Moore/Bevin/284th	A 0.4 0.000	A 0.4 0.000	+ 0.000 V/C
9 61st/Bennet/Main Access	A 2.0 0.000	A 2.0 0.000	+ 0.000 V/C
# 11 Daybreak/Hyatt/269th	A 1.5 0.000	A 1.5 0.000	+ 0.000 V/C
# 13 82nd Ave/279th	A 0.9 0.000	A 0.9 0.000	+ 0.000 V/C

Filename: SMEXAM.OUT 07/21/1998 12:07 Page 2-1 Tue Jul 21, 1998 11:43:34 SMEXAM, CND . -----Daybreak Mine Existing Traffic Volumes AM Peak Hour Level Of Service Computation Report 1994 HCM Unsignalized Method (Base Volume Alternative) Intersection #2 Moore/Bevin/284th ************************************* Average Delay (sec/veh): 0.4 Worst Case Level Of Service: A North Bound South Bound East Bound West Bound Approach: L - T - R L - T - R L - T - R L - T - R Movement: Uncontrolled Uncontrolled Stop Sign Stop Sign Control: Include Include Include Include Rights: 0 0 1 0 0 0 0 0 0 0 1 0 0 0 0 0 0 1 0 0 Lanes: THE STATE OF THE S Volume Module: 0 9 0 0 19 0 0 0 0 Base Vol: Initial Bse: 0 9 0 0 19 0 0 0 0 4 0 0 0 0 5 0 PHF Volume: 0 12 0 0 26 0 0 0 0 0 0 0 0 12 0 0 26 0 0 ٥ Reduct Vol: 0 0 0 5 0 Final Vol.: Adjusted Volume Module: 0% 0% 0% Grade: XXXX XXXX % Cycle/Cars: 0.00 0.84 XXXX Truck/Comb: 0.16 0.00 XXXX XXXX XXXX XXXX Cycl/Car PCE: 0.50 1.00 XXXX XXXX XXXX XXXX XXXX XXXX Trak/Cmb PCE: 1.50 2.00 XXXX XXXX 5 0 0 Adj Vol.: 0 12 0 0 26 0 0 0 0 Critical Gap Module: ••••••| Capacity Module: *********** Level Of Service Module: Shared LOS: * * * * * * * * * *

Page

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0.0

ApproachDel:

0.0

0.0

Filename: SMEXAM.OUT

Approach:

Tue Jul 21, 1998 11:43:34

West Bound

Page 5-1

Page 5

Daybreak Nine Existing Traffic Volumes AM Peak Hour

Level Of Service Computation Report 1994 MCM Unsignalized Method (Base Volume Alternative)

East Bound

L - T - R

Intersection #13 82nd Ave/279th (verage Delay (sec/veh): 0.9 Worst Case Level Of Service:

L - T - R

North Bound South Bound

0.3

ApproachDel:

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ese Vol: rowth Adj:	1.0	3 0 :	17 1.00	1	. 00	•	_	1.00	1.00		1.00	1.00		1.00	1.00
nitial Bee:		3	17 1.00		00	1.1	2	136 1.00	1.00	1.00	1.00			1.00	1.0
er Mj: F Mj:			0.93	_	. 93		93	0.93		0.93	0.93	0.93	0.93	0.93	0.9
T Volume:	:	3	18		4	<u> </u>	2		0	0	_		ő	ŏ	ì
educt Vol: inal Vol.:	:	3	18		4		2	-	1		5	23	17	0	. (

Adjusted Volume Module:	0%	0%	04
Trade: 00 0.89 t Cycle/Cars: 0.00 0.89 t Truck/Comb: 0.11 0.00 PCE Adj: XXXX 1.00 1.00 Cycl/Car PCE: 0.80 1.00 Trock/Cab PCE: 1.50 2.00 Adj Vol.: 3 18	0.00 0.96 0.04 0.00 0.50 1.00 0.50 1.00 1.50 2.00	XXXX XXXX XXXX XXXX 0 6 25	0.50 1.00 1.50 2.00 17 0 0
Critical Gap Module:			

HOVEUD Time: 2.1 EXEX EXEXX 2.1 EXEX EXEXX EXEXX 3.3 2.6 3.4 EXEX EXEXX Critical Op: 5.0 EXEX EXEXX 5.0 EXEX EXEXX Capacity Module: Cnflict Vol: 147 MARK MARKE 23 MARK MARKE 175 147 187 MARK MARKE Potent Cap.: 1458 MARK MARKE 1672 MARK MARKE 283 1167 826 MARK MARKE

Adj Cap: 1.00 EXER EXERT 1.00 EXER EXERT EXERT EXERT 1.00 1.00 0.97 EXER EXERT EXERT HOVE Cap.: 1456 EXER EXERT 1672 EXER EXERT EXER

Level Of Service Module: Stopped Del: 2.5 xxxx xxxxx 2.2 xxxx xxxxx xxxxx 4.1 3.1 4.6 xxxx xxxxx LOS by Hove: A * * A * * * A * * * Hovement: LT - LTR - RT LT - LTR - RT LT - LTR - RT 3.3

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0.0

verage Delay (sec/veh): 1.5

Davbreak Mine Existing Traffic Volumes PM Peak Hour

Level Of Service Computation Report

1994 HCM Unsignalized Method (Base Volume Alternative) ***************

ntersection #9 61st/Bennet	E/Main Acces	****	*
Delaw (eeg/web):	1.8	Worst Case Level Of Service:	

verage Delay	(80	s/veh)		1.5		W o	TSC CE	180 L	ABT OT	94444 *****	****	*****
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nitial Boo:	11	23	0	0	14	3	1.00	•		_		
mer Adj:	1.00	1.00	-	1.00	0.81	0.81	0.81	0.81	0.81	0.81		
	14		0	0		5	Ö	0	0	Ö	ō	0
inal Vol.:	14			0	17	5	7 	0	30 			
dinated Volu	ume M	odule	:	11		'			•		•	

djusted Volume	O#	04	0%	0%
Truck/Comb:	0.00 0.85 0.15 0.00	XXXX XXXX	0.00 0.68 0.32 0.00	XXXX XXXX XXXX XXXX 1.10 1.10 1.10
yel/Car PCE: trok/Cab PCE:	0.50 1.00 1.50 2.00	XXXX XXXX XXXX XXXX	0.50 1.00 1.50 2.00	XXXX XXXX 0 0 0
ritical Cap No	dule:			XXXXX XXXX XXXXX

ritical Op: 5.0 XXXX XXXX XXX		
'apacity Module: 'mflict Vol: 22 xxxx xxxxx xx	XXX XXXX XXXXX 62 X	XXX 20 XXXX XXXX XXXX XXX 1363 XXXX XXXX XXXX
iotent Cap: 1673 MAX MAXX M idj Cap: 1.00 MAXX MAXX M fove Cap: 1673 MAX MAXX M	*** YYYY YYYYT U.YY X	XXX 1.00 XXXX XXXX XXXXX XXX 1353 XXXX XXXX XXXXX

ove Cap		1673 XXX	x xxxx	 ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	 	 		
	• • • • • • •	ice Modu	• • •					

level Of Service Module: stopped Del: 2.2 REEK REGIES OF by Move: A * * * * * * * * * * * * * * * * * *	LT - LTR	- RT LT XXXXX XXXX XXXXX XXXXX	- LTR - RT	LT - LTR - RT
---	----------	--------------------------------------	------------	---------------

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Mon Jul 20, 1998 08:08:42

07/20/1998 08:32

Daybreak Mine Existing Traffic Volumes PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Base Volume Alternative) Page 4

Page 4-1

Intersection #11 Daybreak/Hyatt/269th ************************* Average Delay (sec/veh): 0.6 Worst Case Level Of Service: A ***************************

East Bound West Bound Approach: North Bound South Bound L - T - R L - T - R L - T - R Uncontrolled Uncontrolled Stop Sign Stop Sign Control: Include Include Include Rights: Include 0 1 0 0 0 0 0 0 1 0 0 0 11 0 0 0 0 0 0 ***********

Volume Module: 0 0 87 1 1 0 22 0 0 45 252 Base Vol: Initial Bse: 45 252 0 0 87 1 1 0 22 0 0 0 PHF Adj:

Adjusted Volume Module: 0% +4% -49 Grade: XXXX XXXX 0.00 0.85 0.00 0.91 % Cycle/Cars: 0.00 0.96 XXXX XXXX 1 Truck/Comb: 0.04 0.00 0.09 0.00 0.15 0.00 XXXX XXXX 0.50 1.00 Cycl/Car PCE: 0.70 1.40 0.30 0.80 XXXX XXXX 1.50 2.00 Trok/Cmb PCE: 3.00 6.00 1.00 1.20 0 0 0 1 0 28 0 101 1 Adj Vol.: 77 293 0

Critical Gap Module: Critical Gp: 5.0 EXEX XXXXX XXXXX XXXXX 6.5 XXXX 5.5 XXXXX XXXX Capacity Module: Cofflict Vol: 102 XXXX XXXXX XXXX XXXX XXXX 447 XXXX 102 XXXX XXXX Potent Cap.: 1532 XXXX XXXXX XXXX XXXX XXXXX XXXXX

Level Of Service Module: Stopped Del: 2.4 XXXX XXXXX XXXXX XXXX XXXX 6.6 XXXX 3.0 XXXXX XXXX XXXX Shared LOS: * * * A * * 0.0 3.1 0.5 ApproachDel:

ApproachDel:

7/21/1998 12:13 Tue Jul 21, 1998 11:49:01

SPEAKL.CHD

Page 1-1

Daybreak Mine Existing Plus Project Traffic Volumes - with conveyor AM Peak Hour

Impact Analysis Report Tevel Of Service

-							
ntersection		Base Del/ V/		Future Del/ V/	Change in		
		Veh C		Veh C	+ 0.000 V/C		
2 Moore/Bevin/284th	λ	0.4 0.000	A	0.4 0.000	+ 0.000 1/4		
9 61st/Bennet/Main Access	λ	2.0 0.000	λ	2.1 0.000	+ 0.000 V/C		
11 Daybreak/Hyatt/269th	λ	1.5 0.000	λ	1.7 0.000	+ 0.000 V/C		
13 22nd Ave/279th	λ	0.9 0.000	λ	0.9 0.000	+ 0.000 V/C		

Page 2-1 Tue Jul 21, 1998 11:49:01 SHPPAN1.CHD -----Daybreak Mine Existing Plus Project Traffic Volumes - with conveyor AM Peak Hour Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) Intersection #2 Moore/Bevin/284th ****************************** Average Delay (sec/veh): 0.4 Worst Case Level Of Service: A North Bound South Bound East Bound West Bound L - T - R L - T - R L - T - R Approach: Movement: -------Uncontrolled Uncontrolled Stop Sign Stop Sign Control: Include Include Rights: Lanes: Volume Module: 0 0 0 9 0 0 19 0 Base Vol: 4 0 0 Initial Bse: 0 9 0 0 19 0 0 0 0 ٥ 0 Added Vol: 0 ٥ 0 0 0 2 0 0 3 PasserByVol: 0 Ω ٥ ٥ 0 21 0 Initial Fut: 0 12 PHF Adj: 0 0 0 5 0 0 PHF Volume: 0 16 0 0 29 0 0 0 0 0 0 0 16 0 0 0 0 0 Reduct Vol: 0 0 29 Final Vol.: Adjusted Volume Module: 0% 0.0 Grade: 0% XXXX XXXX XXXX XXXX XXXX XXXX % Cycle/Cars: 0.00 0.84 XXXX XXXX XXXX XXXX * Truck/Comb: 0.16 0.00 XXXX XXXX XXXX XXXX Cycl/Car PCR: 0.50 1.00 XXXX Trok/Cmb PCE: 1.50 2.00 5 0 0 0 0 0 0 0 29 0 0 16 Adj Vol.: Critical Gap Module: MoveUp Time: REKKE KERK KERKE KERKE KERKE KERKE KERKE KERKE 3.4 KEKK KERKE ••••••| Capacity Module: Level Of Service Module: Movement: LT - LTR - RT Shared LOS: * * * * * * * * * * * 0.0

Filename: SMPPAM1.CUT

7/21/1999 12:13

Page 5-1 Tue Jul 21, 1998 11:49:01 MPPARI.CRD

Daybreak Mine Existing Plus Project Traffic Volumes - with conveyor AM Peak Hour

Level Of Service Computation Report 1994 MCM Unsignalized Method (Future Volume Alternative) intersection #13 82nd Ave/279th Worst Case Level Of Service: werage Delay (sec/veh): 0.9 East Bound North Bound south Bound pproach: L-T-R L-T-R L-T-R L - T - R lovement: Stop Sign Uncontrolled Uncontrolled : lortnot Include Include Include Include tights: 0 0 11 0 0 0 0 0 1 0 1 0 0 0 0 0 11 0 0 folume Module: 5 21 2 136 1 ٥ tage Vol: 21 2 136 1 0 Initial Boo: 3 17 4 a 0 ٥ ٥ ٥ 0 0 0 wided Vol: ۵ ٥ 0 ٥ PRESENTEVVOL: 1 ٥ 5 21 16 0 2 137 1 3 18 nitial Put: 0.93 mp adj: 0 5 23 17 3 19 2 147 1 4 'MF Volume: 0 0 0 0 0 0 0 0 0 0 teducts Vol: 3 19 23 17 2 147 Minal Vol.: Mjusted Volume Module: 09 01 03 zrađe: 0.00 0.98 XXXX XXXX) Cycle/Cars: 0.00 0.89 0.00 0.96 XXXX XXXX 0.02 0.00 0.04 0.00 t Truck/Comb: 0.11 0.00 PCB Adj: MXXX 1.00 1.00 MXXX 1.00 1.00 1.10 1.10 1.10 MXXX MXXX 0.50 1.00 0.50 1.00 XXXX XXXX Cycl/Car PCE: 0.50 1.00 1.50 2.00 XXXX XXXX Prot/Cmb PCE: 1.50 2.00 1.50 2.00 0 6 25 2 147 1 3 19 4 Naj Vol.: mitical Cap Hodule: toveUp Time: 2.1 NXXX XXXXX 2.1 NXXX XXXXX XXXXX 3.3 2.6 3.4 XXXX XXXXX Tritical Gp: 5.0 MUX XXXXX 5.0 XXXX XXXXX 6.0 5.5 6.5 MUX XXXXX Capacity Module: Inflict Vol: 148 HXXX XXXXX 24 XXXX XXXXX XXXX 177 148 189 XXXX XXXXX Potent Cap.: 1457 XXXX XXXXX 1670 XXXX XXXX XXXX 881 1165 823 XXXX XXXX Adj Cap: 1.00 NEEK NEEK 1.00 NEEK NEEK 1.00 1.00 0.97 NEEK NEEK Nove Cap.: 1457 REER REERE 1670 REERE REERE REERE 878 1165 799 REERE REERE Level Of Service Module: Stopped Del: 2.5 NXXX XXXXX 2.2 XXXX XXXXX XXXXX 4.1 3.2 4.6 XXXX XXXXX

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ApproachDel:

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Filename: SMPPAM1.OUT

Page 4-1

NPPPN1.CHD

ApproachDel:

0.9

Tue Jul 21, 1998 11:56:43

Daybreak Mine

Existing Plus Project Traffic Volumes - with conveyor PM Peak Hour

Level Of Service Computation Report

1994 MCM Unsignalized Method (Future Volume Alternative)

intersection #9 61st/Bennet/Main Access *********************************** (verage Delay (seg/veh): 1.6 Worst Case Level Of Service: A

**********			*****	*****	****	****	*****	****	****	****	****	*****
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										1		
control:		contro		. One	ontro	lled	Sto	op Si	gn		op 8:	
	OH				Inclu			Inclu	de		Incli	
tights:		Inclu			0		^ ^	11	0 0	0 0	0	0 0
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							1					•
/olume Hodule											_	0
lace Vol:	11	23	0	0	14	4	6	0	24	0	. 0	•
movth Adi:		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
			2.00	0	14	4	6	0	24	0	0	0
mitial Bso:	11	23	-	•	0	ō	ŏ	ō	0	0	0	0
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PassexByVol:	3	0	0	0	0	1	1	_		•	ō	Ă
mitial Fut:	14	23	0	0	14	5	7	0	31	0	-	
Jeer Adi:		1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00		
		0.81	0.81	0.81		0.81	0.81	0.81	0.81	0.81	0.81	0.81
ar vel:				0.00	17	6	9	0	38	0	0	0
'HF Volume:	17	28	0	_		ŏ	ō	ŏ	ō	0	0	0
: LoV'spubes	. 0	_	0	0	0	•	و	_	38	ŏ	ō	٥
rinal Vol.:	17	28	0	0	17	6	,	·	30	. •	•	•
idjusted Vol	ume M	odule	:									
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	-		0.00	223	CCC 2	XXXX	0.	32 (0.00	X 2	CXX .	XXXX
t Truck/Comb				1.10			****	TTTT	XXXXX	1.10	1.10	1.10
		1.00							L.00		CXX	
Cycl/Car PCE			1.00		ccc :			50 2			CCC	
Irek/Cub PCE	: 1	.50	2.00	20	CC :					~		
Add Vol.:	19	28	0	0	17	6	10	0	44	٠,	•	•
mitical Cap	Modu	10:										
toveUp Time:	2 1		TTTTT	TXXXX	XXXX	XXXXX	3.4	XXXX				XXXXX
								XXXX	5.5	XXXXX	XXXX	XXXXX
mitical op:	. 5 .u	XXXX	****		~~~		1			1		
	1			11			•			•		•
Capacity Mod	ale:								20		****	XXXXX
miliet Vol:		****	XXXXX			XXXXX		XXXX				
Potent Cap.:	1671	XXXX	XXXXX	XXXX	XXXX	XXXXX		XXXX				XXXXX
	1 00	TTTT	XXXXX	XXXX	XXXX	XXXXX	0.99	XXXX				XXXX
Adj Cap:							959	XXXX	1352	XXXX	XXXX	XXXXX
Nove Cap.:	10/1		****	حججها ا			11					
	1			11			1.6			•		·
Level Of Ser	Vice	Modul	•:						2 7		***	XXXXX
Stopped Del:	2.2	XXXX	XXXXX	XXXXX	XXXX	XXXXX	3.8	XXXX	4.7	****		
LOS by Nove:		•	*	•	*	*	*				·-	
Movement:		- LTR	- RT	LT ·	- LTR	- RT			- RT			- RT
MOARMAILE I	-							1287	TTTTT	XXXX	XXXX	XXXXX

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Shrd StpDel: REGER REEK REKER REGER REGER REGER REGER REGER REGER REGER REGER

Shared LOS:

Daybreak Mine Existing Plus Project Traffic Volumes - with conveyor

PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

Tue Jul 21, 1998 11:56:43

Intersection #11 Daybreak/Hyatt/269th ************************** Average Delay (sec/veh): 0.6 Worst Case Level Of Service: A Approach: North Bound South Bound East Bound West Bound L - T - R L - T - R L - T - R Stop Sign Stop Sign Uncontrolled Uncontrolled Control: Include Include Include Include Rights: 0 1 0 0 0 0 0 0 1 0 0 0 11 0 0 0 0 0 0 Volume Module: 0 0 87 1 1 0 22 0 0 Base Vol: 45 252 Initial Bse: 45 252 0 0 87 1 1 0 22 0 0 0 0 0 0 ٥ Added Vol: 0 0 PasserByVol: 3 0 0 0 0 0 1 0 6
Initial Fut: 48 252 0 0 87 1 2 0 28 0 0 0 0 0 PHF Volume: 56 293 0 0 101 1 2 0 33 0 0 Reduct Vol: 0 0 0 0 0 0 0 0 0 0 0 ٥ Reduct Vol: 0 0 0 Final Vol.: 56 293 0 0 101 1 2 0 33 0 Adjusted Volume Module: -4% Grade: +49 0.00 0.85 XXXX XXXX % Cycle/Cars: 0.00 0.96 0.00 0.91 xxxx xxxx 0.15 0.00 0.09 0.00 Truck/Comb: 0.04 0.00 XXXX XXXX 0.30 0.80 0.50 1.00 Cycl/Car PCE: 0.70 1.40 XXXX XXXX 1.50 2.00 1.00 1.20 Trck/Cmb PCE: 3.00 6.00 0 101 1 3 0 35 0 0 0 Adj Vol.: 82 293 0 Critical Gap Module: MoveUp Time: 2.1 XXXX XXXXX XXXXX XXXX XXXXX 3.4 XXXX 2.6 XXXXX XXXX Critical Op: 5.0 XXXX XXXXX XXXXX XXXXX XXXXX 6.5 XXXX 5.5 XXXXX XXXX Capacity Module: Chflict Vol: 102 XXXX XXXXX XXXX XXXX XXXX 451 XXXX 102 XXXX XXXX XXXX Potent Cap.: 1532 XXXX XXXXX XXXX XXXX XXXXX 581 XXXX 1230 XXXX XXXX Adj Cap: 1.00 XXXX XXXXX XXXX XXXX XXXXX 0.94 XXXX 1.00 XXXX XXXX XXXX Move Cap.: 1532 XXXX XXXXX XXXX XXXX XXXX 543 XXXX 1230 XXXX XXXX XXXX Level Of Service Module: Stopped Del: 2.4 XXXX XXXXX XXXXX XXXXX XXXXX 6.7 XXXX 3.0 XXXXX XXXXX Shrd StpDel:xxxxx xxxx xxxxx xxxxx xxxxx xxxxx 3.3 xxxxx xxxxx xxxxx Shared LOS: * * * * * * * * * * * * * * *

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0.0

0.5

ApproachDel:

3.3

(PPAN2.IN

Tue Jul 21, 1998 11:59:12

Page 1-1

Daybreak Nine Existing Plus Project Traffic Volumes - no conveyor

AM Peak Hour Impact Analysis Report Level Of Service

		Base		Futt	ire	Change		
atersection		Del/ V/		Del/	V/	in		
	LOS	Veh C		Veh	C			
2 Hoore/Bevin/284th	λ	0.4 0.000	λ	0.4	0.000	+ 0.000 V/C		
9 61st/Bennet/Main Access	A	2.0 0.000	A	2.0	0.000	+ 0.000 V/C		
11 Daybreak/Hyatt/269th	λ	1.5 0.000	A	1.5	0.000	+ 0.000 V/C		
13 82nd Ave/279th	A	0.9 0.000	A	0.9	0.000	+ 0.000 V/C		

Tue Jul 21, 1998 11:59:12 Page 2-1 Daybreak Mine Existing Plus Project Traffic Volumes - no conveyor AM Peak Hour Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) Intersection #2 Moore/Bevin/284th **************************** Average Delay (sec/veh): 0.4 Worst Case Level Of Service: A Approach: North Bound South Bound East Bound Movement: L - T - R L - T - R L - T - R L - T - R Control: Uncontrolled Uncontrolled Stop Sign Stop Sign Include Include Rights: Volume Module: 0 9 0 0 19 0 Initial Bse: 0 9 0 0 19 0 0 0 0 4 0 0 Added Vol: 0 0 0 0 0 0 0 0 0 0 0 0 0 ٥ 0 PasserByVol: 0 0 0 0 0 0 0 0 0 0 4 Initial Fut: 0 9 0 0 19 0 Ω 0 0 0 5 0 ٥ PHF Volume: 0 12 0 0 26 0 ۵ 0 0 0 0 0 0 0 0 0 0 Reduct Vol: 5 0 0 12 0 0 26 Final Vol.: Adjusted Volume Module: -4% 0% 0% Grade: XXXX XXXX XXXX XXXX % Cycle/Cars: 0.00 0.84 XXXX XXXX XXXX XXXX * Truck/Comb: 0.16 0.00 XXXX XXXX XXXX XXXX XXXX XXXX Cycl/Car PCE: 0.50 1.00 XXXX XXXX XXXX XXXX XXXX XXXX XXXX XXXX Trok/Cmb PCE: 1.50 2.00 XXXX XXXX 0 12 0 0 26 0 0 0 0 5 0 0 Adj Vol.: Critical Gap Module: MOVEUR Time: REKKE KEKKE KEKKE KEKKE KEKKE KEKKE KEKKE KEKKE 3.4 KEKKE KEKKE Capacity Module: Level Of Service Module: ApproachDel:

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HPPAH2.IN

Shared LOS: * *

ApproachDel:

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Tue Jul 21, 1998 11:59:12

Daybreak Mine Existing Plus Project Traffic Volumes - no conveyor

AM Peak Hour

Level Of Service Computation Report 1994 MCM Unsignalized Method (Future Volume Alternative) intersection #13 82nd Ave/279th

Worst Case Level Of Service: verage Delay (sec/veh): 0.9 North Bound South Bound East Bound West Bound pproach: L-T-R L-T-R L - T - R L - T - R lovement: Stop Sign Stop Sign Uncontrolled Uncontrolled ontrol: Include Include Include Include tighte: 1 0 0 0 0 0 0 11 0 0 0 0 0 1 0 0 0 11 0 0 folume Module: 2 136 0 5 21 17 tage Vol: 16 21 2 136 1 0 mitial Bse: 3 17 ۵ ٥ 0 ٥ udded Vol: 0 0 0 0 0 . 'asserByVol: ٥ 21 16 5 2 136 3 17 4 initial Put: mp adj: 0 5 Ω 3 18 4 2 146 1 'HF Volume: ٥ 0 Ω 0 0 0 0 teduct, Vol: 0 17 Λ ٥ 2 146 3 18 Minal Vol.: Mjusted Volume Module: 01 0% 04 Trade: 0.00 0.98 XXXX XXXX 0.00 0.96 : Cycle/Cars: 0.00 0.89 0.02 0.00 0.04 0.00 XXXX XXXX 1 Truck/Comb: 0.11 0.00 0.50 1.00 XXXX XXXX Cycl/Car PCE: 0.50 1.00 0.50 1.00 1.50 2.00 XXXX XXXX 1.50 2.00 Frek/Cmb PCE: 1.50 2.00 0 0 17 0 6 25 2 146 1 3 18 voj vol.: mitical Cap Module: toveUp Time: 2.1 MANN MANNN 2.1 MANN MANNN MANNN 3.3 2.6 3.4 MANN MANNN tritical Op: \$.0 MANN NAMEN 5.0 MANN NAMEN 6.0 5.5 6.5 MANN NAMEN :apacity Module: Inflict Vol: 147 MANN MANNE 23 MONN MONNE 175 147 187 MANN MANNE POTENT Cap.: 1458 MANN MANNE 1672 MANN MONNE MANN 883 1167 826 MANN MANNE tore Cap.: 1458 EXXX EXXXX 1672 EXXX EXXX EXXX 880 1167 802 EXXX EXXXX Level Of Service Module: Stopped Del: 2.5 MRMM MANNE 2.2 MANN MANNE MANNE 4.1 3.1 4.6 MANN MANNE LOS by Hove: A * * A * * * A *

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Shared Cap.: MAXX MAXX MAXXX MAXX MAXX MAXXX MAXXX MAXXX MAXXX MAXXX Shard StepDel: NOONE NAME ANNAN ANNAN ANNAN ANNAN ANNAN ANNA ANNAN ANNA ANNAN •

LT - LTR - RT LT - LTR - RT LT - LTR - RT LT - LTR - RT

.

3.3

λ

Filename: SMPPAM2.OUT

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SMPPPM2.IN

1/21/1998 12:26

apacity Module:

evel Of Service Module:

(PPPM2.IN

Tue Jul 21, 1998 12:01:46

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West Bound

Page

Daybreak Nine Existing Plus Project Traffic Volumes - no conveyor PM Peak Hour

.................. Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

Rast Bound

itersection #9 61st/Bennet/Main Access Worst Case Level Of Service: rerage Delay (sec/veh): 1.8

South Bound

North Bound proach: L - T - R L - T - R L - T - R : Inement: Stop Sign Stop Sign Uncontrolled Uncontrolled : lorznc Include Include Include Include ights: 0 0 0 0 0 0 0 11 0 0 0 0 0 1 0 0 1 0 0 0 IDOS: olume Module: 0 14 11 23 ase Vol: 0 0 24 ٥ 0 0 14 nitial Bse: 11 23 0 ٥ 0 0 ided Vol: • ٥ 10 Ω 0 asserByVol: ٥ ٥ 11 16 ٥ 0 14 nitial Put: 15 23 1.00 1.00 1.00 1.00 1.00 ser Adj: 1.00 1.00 1.00 1.00 1.00 0.81 0.81 0.81 0.81 0.81 0.81 0.81 0.81 0.81 0.81 IF Adj: 41 ٥ 0 20 C IF Volume: 19 28 0 17 14 0 ٥ 0 ٥ 0 ٥ 0 0 educt Vol: 0 ٥ n inal Vol.: 19 28 20 0 0 17 14 djusted Volume Module: 0% 01 0% XXXX XXXX 0.00 0.68 Cycle/Cars: 0.00 0.85 XXXX XXXX XXXX XXXX 0.32 0.00 XXXX XXXX Truck/Comb: 0.15 0.00 CE Adj: XXXX XXXX 0.50 1.00 XXXX XXXX yel/Car PCB: 0.50 1.00 1.50 2.00 XXXX XXXX XXXX XXXX rck/Cmb PCE: 1.50 2.00 0 47 ٥ ٥ 0 17 14 23 aj Vol.: 20 28 ritical Gap Module: OVEUD Time: 2.1 XXXX XXXXX XXXXX XXXXX 3.4 XXXX 2.6 XXXXX XXXX

topped Del: 2.2 KKKK KKKKK KKKKK KKKKK XKKKK 3.9 KKKK 2.8 KKKKK KKKK KKKKK OS by Hove: A * * * * * * * Ovement: LT - LTR - RT had StyDel: XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX 3.2 XXXXX XXXXX XXXXX

ritical Op: \$.0 REEK MEEKS MAKEN MAKEN MAKEN 6.5 REEK S.S MEEKS MAKEN MAKEN

nflict Vol: 21 MANN MANNA MANN MANNA otent Cap.: 1687 MANN MANN MANN MANN MANN 963 MANN 1346 MANN MANN MANN

* * * * * A hared LOS: * 0.0 3.1 0.9 pproachDel:

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Filename: SMPPPM2.OUT

Tue Jul 21, 1998 12:01:46 --------

Daybreak Mine Existing Plus Project Traffic Volumes - no conveyor PM Peak Hour

Level Of Service Computation Report

1994 HCM Unsignalized Method (Future Volume Alternative)

Intersection #11 Davbreak/Hvatt/269th

Intersection #11 Daybreak/Hyatt/209th												
Average Delay	. /	- /b \				Vac	rat C	as L	evel Of	Servi	ce :	λ
WALEGO DOTEM	1880	3/ V O II/	: +	*****	****	*****	****	****	*****	*****	****	*****
		rth Bo			ith B				bauc	We	st Bo	und
ypproach:	•	-		• •	. T	- 9	t.	- Т	- R		T	
Movement:	- سر 	- <u>.</u>	1	1								
		contro	33.4	Had	ont w	olled	S1	top S	ian	'' st	op Si	gn
Control:	Une	Inclu		Olic	Incl			Incl			Inclu	
Rights:		Tuero		0 (1 0			0 0	0 0	0	0 0
Lanes:												
				1			1 1			• •		
Volume Module		252	0	٥	87	1	1	٥	22	0	0	0
Base Vol:	45	1.00			1.00	_	1.00			1.00	1.00	1.00
Growth Adj:	45	252	1.00	1.00	87	1.00	1		22	0	0	0
Initial Bso:	40	252	ŏ	ă	ő	-	0	ō	0	0	0	0
Added Vol:	-	٥	ő	٥	ő	ŏ	i	ō	8	0	0	0
PasserByVol:	_	252	ŏ	ŏ	87	ĭ	2	-	30	0	0	0
Initial Fut:		1.00	_	1.00			_	1.00	1.00	1.00	1.00	1.00
User Adj:		0.86	0.86		0.86	0.86		0.86	0.86	0.86	0.86	0.86
PHF Adj: PHF Volume:		293	0.20	0.00	101	1	2		35	0	0	0
Reduct Vol:	3/		ŏ				0	0	0	0	0	0
Final Vol.:	57	-	ŏ	-	101	1	2	0	35	0	0	0
Adjusted Volu			-	•		-						
Grade:	AHIG 17	+49			-48			0%			0%	
% Cycle/Cars:		.00	. 96	٥	.00	0.91	0	.00	0.85	xx	xx x	XXX
* Truck/Comb		.04		ō	.09	0.00	0	. 15	0.00		xx x	
			1.00	XXXX	1.00	1.00	XXXX	XXXX	XXXXX	1.10	1.10	1.10
Cvcl/Car PCE:		.70 1			.30			.50	1.00	XX	xx x	XXX
Trok/Cmb PCE		.00			.00		1	.50	2.00	XX	xx x	XXX
Adi Vol.:		293				1	3	0	38	0	0	0
Codedgel Gen	Modu	10:										
MoveUp Time:	2.1	XXXX	xxxxx	XXXXX	XXXX	XXXXX	3.4	XXXX		XXXXX		
muladan ma			****	TTTTT	TYXX	TXXXX	6.5	XXXX	5.5	XXXXX		
CLIFICAL OD:	1											
Canadity Modi	ile:											
Cofflict Vol:	102	XXXX	XXXXX	XXXX	XXXX	XXXXX	452	XXXX	102			XXXXX
Potent Cap.:	1532	XXXX	XXXXX	XXXX	XXXX	XXXXX	580	XXXX	1230			XXXXX
Adi Cap:	1.00	XXXX	XXXXX	XXXX	XXXX	XXXXX	0.93	XXXX				XXXXX
M	1633			****	TTTT	TTTTT	542	XXXX	1230			XXXXX
Move Cap.:				[
Level Of Ser	vice	Module) :									
Stopped Del:	2.4					XXXXX	6.7	xxxx	3.0	XXXXX	XXXX	****
LOS by Move:		*				*	*		- 50		LTR	_
Movement:	LT	- LTR	- RT	LT	- LTR	- RT	LT	- LIR	- RT			
Shared Cap.:	XXXX	XXXX	XXXXX	XXXX	XXXX	XXXXX	XXXX	1133	*****	****	****	YYYYY
Shared Cap.: Shrd StpDel::			XXXXX	XXXXX	XXXX	XXXXX	****	. 3.3 A	****	*	*	+
Shared LOS:	*	*	*	•	0.0		-	3.2	-		0.0	
ApproachDel:		0.5			0.0			3.2				

Daybreak Hine Future (1999) Base Traffic Volumes AM Peak Hour

Impact Analysis Report Level Of Service

Intersection	Base	Future	Change		
	Del/ V/ LOS Veh C	Del/ V/ LOS Veh C	in		
# 2 Moore/Bevin/284th	A 0.4 0.000	A 0.4 0.000	+ 0.000 V/C		
# 9 61st/Bennet/Hain Access	A 2.0 0.000	A 2.0 0.000	+ 0.000 V/C		
# 11 Daybreak/Hyatt/269th	A 1.6 0.000	A 1.6 0.000	+ 0.000 V/C		
# 13 82nd Ave/279th	A 0.9 0.000	λ 0.9 0.000	+ 0.000 V/C		

Page 2-1 Thu Aug 20, 1998 14:35:24 SMFTANB.CHD Davbreak Mine Future (1999) Base Traffic Volumes AM Peak Hour Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) **************************** Intersection #2 Moore/Bevin/284th ************************** Average Delay (sec/veh): 0.4 Worst Case Level Of Service: North Bound South Bound East Bound L - T - R L - T - R L - T - R L - T - R Movement: Stop Sign Uncontrolled Stop Sign Uncontrolled Control: Include Include Include Include Rights: 1 0 0 0 0 0 0 1 0 0 0 0 0 0 Lanes: 0 0 1 0 0 .|-----||------| -----Volume Module: Base Vol: 0 9 0 0 19 0 ٥ 0 0 4 Initial Bse: 0 9 0 0 19 n 0 0 0 0 Added Vol: ٥ n ۵ ٥ ٥ 0 ٥ n PasserByVol: ٥ 19 ۵ Initial Put: 0 9 0 0 0 PHF Volume: 0 13 0 0 27 0 0 0 ٥ 0 ۵ Reduct Vol: 0 0 Ω n 0 ٥ 0 13 27 ٨ Final Vol.: Adjusted Volume Module: -44 0% Grade: 0% XXXX XXXX XXXX XXXX % Cycle/Cars: 0.00 0.84 XXXX XXXX XXXX XXXX XXXX XXXX XXXX XXXX * Truck/Comb: 0.16 0.00 XXXX XXXX XXXX XXXX XXXX XXXX Cycl/Car PCE: 0.50 1.00 XXXX XXXX Trok/Cmb PCE: 1.50 2.00 XXXX XXXX XXXX XXXX 0 27 0 5 0 0 0 0 0 13 0 Adj Vol.: Critical Gap Module: Capacity Module: Cnflict Vol: XXXX XXXX XXXXX XXXX XXXX XXXXX XXXXX 39 XXXX XXXXX Level Of Service Module: LOS by Move: * * * * * * * * A * * Movement: LT - LTR - RT Shared LOS: * * * * * * * 0.0 3.6 0.0 ApproachDel: 0.0

Filename: SNFTAMB.OUT

08/20/1998 15:01

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SHFTARE.CHD

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Daybreak Nine Puture (1999) Base Traffic Volumes

AM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

**********	*****	********	
Intersection #13 #2nd Ave/27	9th		
*********	******	******	
Average Delay (sec/veh):	0.9	Worst Case Level Of Service:	A

Approach:	North Bound			South Bound			Bast Bound				West Bound												
Mariament .	٠.	_	T		•	L	•	T	-	R	. 1	L	-	T	-	R					<u>.</u>		. 1
Control: Rights:		DC0	ntr ncl	011	.ed	ני	'nc	ont	roll	led	11-		Sto	p i	igr Lude	ı	1	St	:03	9 8	ign ude	1	1
Lanes:	0	0	11	0	0	1	0	1	1 0														۰ ا
Volume Module	:					•				,								16		0		()

Base Vol:	3	17	4	2	136	1	U	5	21	10		
Growth Adj:	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02	1.02
Initial Bee:	3	17	4	2	139	1	0	5	21	16	0	0
Added Vol:	0	0	0	0	0	0	0	0	0	0	0	0
PasserByVol:	ŏ	ō	Ō	0	0	0	0	0	0	0	0	0
Initial Put:	3	17	Ă	2	139	1	0	5	21	16	0	0
User Adj:	1 00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
		0.93	0.93		0.93	0.93	0.93		0.93	0.93	0.93	0.93
PHF Adj:	0.33	19	0.93	2		1.73	00	5.25	23	18	0	0
PHP Volume:	3		•		149	•	,	-	-7	-0	ă	ŏ
Reduct Vol:	0	0	0	0	-	٠		ž	23	18		ň
Pinel Vol .	7	19	4	2	149		U		43	70		•

Final Vol.:	3 19	4	2 143	_				•	•
Adjusted Volume	Module:								
Grade:	0%		0%		0%			08	
% Cycle/Cars:		89	0.00 0.	96	XXXX 2	CCCC		0 0.9	
* Truck/Comb:	0.11 0.	00	0.04 0.		XXXX 3			2 0.0	
PCE Adj: XX	XX 1.00	1.00	xxxx 1.00		1.10 1.10		XXXX X		
Cycl/Car PCE:	0.50 1.	00	0.50 1.	00	XXXX 3	CXXX		0 1.0	
Trek/Cmb PCE:	1.50 2.	00	1.50 2.	00	XXXX 2		1.5		
Adj Vol.:	3 19	4	2 149	1	0 6	25	18	0	0

Adj Vol.: Critical Gap Module: MoveUp Time: 2.1 XXXX XXXXX 2.1 XXXX XXXXX XXXXX 3.3 2.6 3.4 XXXX XXXXX Critical Op: 5.0 XXXX XXXXX 5.0 XXXX XXXXX XXXXX 6.0 5.5 6.5 XXXX XXXXX

Capacity Module: Cnflict Vol: 150 XXXX XXXXX 23 XXXX XXXXX XXXX 178 150 190 XXXX XXXXX Potent Cap.: 1454 XXXX XXXXX 1672 XXXX XXXXX XXXX 880 1163 822 XXXX XXXXX Move Cap.: 1454 XXXX XXXXX 1672 XXXX XXXXX XXXX 876 1163 797 XXXX XXXXX

Level Of Service Module: Stopped Del: 2.5 xxxx xxxxx 2.2 xxxx xxxxx xxxxx 4.1 3.2 4.6 xxxx xxxxx

λ * * * * * * * * Shared LOS: ApproachDel: 0.0

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Filename: SMFTAMB.OUT

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0.0

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Thu Aug 20, 1998 14:37:31 SHIFTIMB.CRD

08/20/1998 15:03

Davbreak Mine Future (1999) Base Traffic Volumes PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) **********

Intersection #9	61st/Bennet/Ma	*****	*******	*****				
Average Delay ((sec/veh) :	1.5 Wo	rst Case Level Of					
Approach:	North Bound	South Bound	East Bound	West Bound				
Morroment : I.	T - R	L-T-R	L-T-R	L - T - R				
			Stop Sign	Stop Sign				
	Uncontrolled Include	Uncontrolled Include	Include	Include				
Rights: 0		0 0 0 1 0	0 0 11 0 0	0 0 0 0 0				
Lanes: 0		[
Volume Module:	•	•						
	11 23 0	0 14 4	6 0 24	0 0 0				
	02 1.02 1.02	1.02 1.02 1.02	1.02 1.02 1.02	1.02 1.02 1.02				
	11 23 0	0 14 4	6 0 24	0 0 0				
Added Vol:	0 0 0	0 0 0	0 0 0	0 0 0				
* #555-51	0 0 0	0 14 4	6 0 24	0 0 0				
	11 23 0 .00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00				
	81 0.81 0.81	0.81 0.81 0.81	0.81 0.81 0.81	0.81 0.81 0.81				
	14 29 0	0 18 5	8 0 30	0 0 0				
Reduct Vol:	0 0 0	0 0 0	0 0 0	0 0 0				
Final Vol.:	14 29 0	0 18 5	8 0 30	0 0 0				
Adjusted Volume			0%	04				
Grade:	04	04	0.00 0.68	XXXX XXXX				
* Cycle/Cars:	0.00 0.85	XXXX XXXX	0.32 0.00	XXXX XXXX				
* Truck/Comb:	0.15 0.00 EXX 1.00 1.00	1.10 1.00 1.00	XXXX XXXX XXXXX	1.10 1.10 1.10				
PCE Adj: XX Cycl/Car PCE:	0.50 1.00	XXXX XXXX	0.50 1.00	XXXX XXXX				
Treft/Cmb PCE:	1.50 2.00	XXXX XXXX	1.50 2.00	XXXX XXXX				
Adi Vol.:	15 29 0	0 18 5	9 0 35	0 0 0				
Critical Gap Mo	odule:							
	2.1 XXXX XXXXX	XXXXX XXXX	• • • • • • • • • • • • • • • • • • • •	XXXXX XXXX XXXXX				
Critical Op: 5	5.0 xxxx xxxx;	***** **** *****						
Capacity Module	B: - 11	XXXX XXXX XXXXX	63 xxxx 20	XXXX XXXX XXXX				
Cnflict Vol:	23 AAAA AAAAA 173 YYYY YYYYY	XXXX XXXX XXXXX	974 xxxx 1352	XXXX XXXX XXXX				
	XXXX XXXX 00.	XXXX XXXX XXXX	0.99 xxxx 1.00	XXXX XXXX XXXXX				
	672 XXXX XXXXX	XXXX XXXX XXXX	965 xxxx 1352	XXXX XXXX XXXXX				
Level Of Service	ce Module:			XXXXX XXXX				
		XXXXX XXXX XXXXX	3.8 xxxx 2.7	* * *				
	* * K	LT - LTR - RT	LT - LTR - RT	LT - LTR - RT				
Movement: L Shared Cap.: XX	LT - LTR - RT	XXXX XXXX XXXXX	XXXX 1252 XXXXX	XXXX XXXX XXXX				
Shed Stabel	haa aaaa aaaaa Yyy yyyx XXXXX :	XXXXX XXXX XXXXX		XXXXX XXXX XXXXX				
SHIR BEDDATIVE			- + A +	* * *				

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2.9

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0.7

Shared LOS:

ApproachDel:

Thu Aug 20, 1998 14:37:31 SMFTPMB.CMD

Davbreak Mine

Filename: SMFTPMB.OUT

Future (1999) Base Traffic Volumes PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

************************ Intersection #11 Daybreak/Hyatt/269th

******************************* Average Delay (sec/veh): 0.6 Worst Case Level Of Service: A West Bound South Bound East Bound North Bound Approach: L-T-R L - T - R L - T - R L - T - R Movement: Stop Sign Stop Sign Uncontrolled Uncontrolled Control: Include Include Include Include Rights: 0 0 0 0 0 1 0 0 0 0 0 0 1 0 0 0 11 0 0 Lanes: Volume Module: 0 87 1 1 0 22 45 252 0 Base Vol: 1 0 22 0 0 89 1 Initial Bse: 46 257 0 0 ۵ ٥ 0 ٥ ٥ 0 0 Added Vol: ٥ 0 0 n PasserByVol: 0 0 ٥ ٥ ٥ ٥ Initial Fut: 46 257 0 89 1 1 0 PHF Adi: 0 0 0 0 103 1 1 0 26 PHF Volume: 53 299 0 0 0 0 0 0 0 Reduct Vol: 0 0 ٥ ٥ 53 299 0 103 n 26 Final Vol.: Adjusted Volume Module: 0% 0% -44 +4% Grade: 0.00 0.85 XXXX XXXX % Cycle/Cars: 0.00 0.96 0.00 0.91 xxxx xxxx 0.09 0.00 0.15 0.00 * Truck/Comb: 0.04 0.00 PCE Adi: XXXX XXXX 0.50 1.00 0.30 0.80 Cycl/Car PCE: 0.70 1.40 1.50 2.00 XXXX XXXX Trck/Cmb PCE: 3.00 6.00 1.00 1.20 1 0 28 78 299 0 0 103 1 Adj Vol.: Critical Gap Module: MoveUp Time: 2.1 xxxx xxxxx xxxxx xxxx xxxx 3.4 xxxx 2.6 xxxxx xxxx xxxxx Capacity Module: Cnflict Vol: 104 xxxx xxxxx xxxx xxxx xxxx 456 xxxx 104 xxxx xxxx xxxx Potent Cap.: 1529 xxxx xxxxx xxxxx xxxxx xxxxx 576 xxxx 1227 xxxx xxxxx xxxxx Adj Cap: 1.00 xxxx xxxxx xxxx xxxx xxxxx 0.94 xxxx 1.00 xxxx xxxx xxxxx Move Cap.: 1529 XXXX XXXXX XXXX XXXX XXXXX 541 XXXX 1227 XXXX XXXXX -----| Level Of Service Module: Stopped Del: 2.4 xxxx xxxxx xxxxx xxxx xxxx 6.7 xxxx 3.0 xxxxx xxxx xxxxx Shrd StpDel:xxxxx xxxxx xxxxx xxxxx xxxxx xxxxx 3.2 xxxxx xxxxx xxxxx xxxxx

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3.2

Shared LOS: * * * * * * A * * *

0.0

0.5

ApproachDel:

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ApproachDel:

SMPTAM1.CMD

SMFTAM1.CMD

Thu Aug 20, 1998 14:08:13

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-Davbreak Mine Future (1999) Plus Project Traffic Volumes - with conveyor AM Peak Hour

Impact Analysis Report Level Of Service

Intersection		Base		Puture	Change
Intersection	Del			Del/ V/	in
	LOS	Veh C	LOS	Veh C	
# 2 Moore/Bevin/284th	A	0.4 0.000	A	0.4 0.000	+ 0.000 V/C
# 9 61st/Bennet/Main Access	λ	2.0 0.000	λ	2.1 0.000	+ 0.000 V/C
* 5 0200/5000000/100000					
# 11 Daybreak/Hyatt/269th	λ	1.6 0.000	A	1.7 0.000	+ 0.000 V/C
# 13 82nd Ave/279th	λ	0.9 0.000	λ	0.9 0.000	+ 0.000 V/C

1994 HCM Unsignalized Method (Future Volume Alternative) Intersection #2 Moore/Bevin/284th ************************ Average Delay (sec/veh): 0.4 Worst Case Level Of Service: A ****************************** Approach: North Bound South Bound East Bound West Bound L-T-R L-T-R L - T - R L-T-R Control: Uncontrolled Uncontrolled Stop Sign Stop Sign Include **Include** Include Include Rights: Lanes: Volume Module: 0 9 0 0 19 0 0 0 0 4 0 Base Vol: Initial Bse: 0 9 0 0 19 0 0 0 4 0 ٥ 0 0 0 0 0 0 0 Added Vol: 0 n n PasserByVol: 0 3 0 0 2 0 0 Initial Fut: 0 12 0 0 21 0 ٥ 0 0 0 0 0 0 6 0 PHF Volume: 0 . 17 0 0 29 0 Reduct Vol: 0 0 0 0 0 0 Final Vol.: 0 17 0 0 29 0 0 ٥ 0 0 Adjusted Volume Module: -44 0% Grade: 0% YYYY XXXX % Cycle/Cars: 0.00 0.84 xxxx xxxx XXXX XXXX Truck/Comb: 0.16 0.00 XXXX XXXX **** *** XXXX XXXX XXXX XXXX XXXX Cycl/Car PCE: 0.50 1.00 XXXX XXXX xxxx xxxx XXXX XXXX XXXX XXXX Trck/Cmb PCE: 1.50 2.00 5 0 0 Adj Vol.: 0 17 0 0 29 0 0 0 0 Critical Gap Module: Capacity Module: Level Of Service Module:

Shared LOS: * * * * * * * * * * *

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0.0

Filename: SMFTAM1.OUT

Thu Aug 20, 1998 14:08:13

AM Peak Hour

Daybreak Mine

Level Of Service Computation Report

Future (1999) Plus Project Traffic Volumes - with conveyor

SHFTAN1.CHD

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Daybreak Mine

Future (1999) Plus Project Traffic Volumes - with conveyor AM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

************************** Intersection #13 \$2nd Ave/279th *************************

Average Delay (sec/veh): 0.9 Worst Case Level Of Service: ************************** North Bound South Bound East Bound Approach: L-T-R L-T-R L - T - R L - T - R Movement: Stop Sign Stop Sign Uncontrolled Uncontrolled Control: Include Include Include Include Lanes: 0 0 11 0 0 0 0 11 0 0 0 0 0 1 0 1 0 0 0 0 Rights: Volume Module: 2 136 1 0 5 21 Base Vol: 3 17

16 0 1 0 5 21 Initial Bse: 3 17 4 2 139 0 ٥ 0 0 ٥ Added Vol: 0 0 0 0 1 ٥ 0 0 0 1 PasserByVol: 16 1 ٥ . 21 4 2 140 Initial Fut: 3 18 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 0.93 PHP Adi: 0 5 23 4 2 150 1 PHF Volume: 3 20 ٥ ٨ 0 0 Ω 0 0 Λ Réduct Vol: 18 n 23 3 20 2 150

Final Vol.: Adjusted Volume Module: 0% 0% Grade: 0.00 0.98 0.00 0.96 XXXX XXXX % Cycle/Cars: 0.00 0.89 XXXX XXXX 0.02 0.00 0.04 0.00 * Truck/Comb: 0.11 0.00 0.50 1.00 0.50 1.00 XXXX XXXX Cycl/Car PCR: 0.50 1.00 1.50 2.00 XXXX XXXX

1.50 2.00 Trck/Cmb PCE: 1.50 2.00 0 6 25 12 0 3 20 4 2 150 1 Adj Vol.: Critical Gap Module:

MoveUp Time: 2.1 XXXX XXXXX 2.1 XXXX XXXXX XXXXX 3.3 2.6 3.4 XXXX XXXXX Critical Gp: 5.0 XXXX XXXXX 5.0 XXXX XXXXX XXXXX 6.0 5.5 6.5 XXXX XXXXX

Capacity Module: Cnflict Vol: 151 xxxx xxxxx 24 xxxx xxxxx xxxx 180 151 192 xxxx xxxxx Potent Cap.: 1452 XXXX XXXXX 1670 XXXX XXXXX XXXX 877 1161 819 XXXX XXXXX

Nove Cap.: 1452 XXXX XXXXX 1670 XXXX XXXX XXXX 874 1161 795 XXXX XXXXX •-----|-----| Level Of Service Module:

Stopped Del: 2.5 XXXX XXXXX 2.2 XXXX XXXXX XXXXX 4.1 3.2 4.6 XXXX XXXXX LOS by Move: A * * A * * * * A * * Movement: LT - LTR - RT LT - LTR - RT LT - LTR - RT

Shared LOS: * * * * * * * * * * * * 4.6 3.4 0.0 0.3 ApproachDel:

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* Truck/Comb: 0.81 0.00 0.06 0.00 0.94 0.00 XXXX XXXX 0.50 1.00 0.50 1.00 Cycl/Car PCE: 0.50 1.00 xxxx xxxx 1.50 2.00 1.50 2.00 Trck/Cmb PCE: 1.50 2.00 Adj Vol.: 66 10 0 0 30 20 26 0 64 0 0 0 Critical Gap Module: MoveUp Time: 2.1 XXXX XXXXX XXXXX XXXXX 3.4 XXXX 2.6 XXXXX XXXX Critical Op: 5.0 XXXX XXXXX XXXXX XXXX XXXX 6.5 XXXX 5.5 XXXXX XXXX •••••••| Capacity Module: Cnflict Vol: 50 xxxx xxxxx xxxx xxxx xxxx 97 xxxx 40 xxxx xxxx xxxxx Potent Cap.: 1623 XXXX XXXX XXXX XXXX 930 XXXX 1322 XXXX XXXX Adj Cap: 1.00 xxxx xxxxx xxxx xxxx xxxxx 0.96 xxxx 1.00 xxxx xxxx xxxxx Move Cap.: 1623 XXXX XXXXX XXXX XXXX XXXX XXXXX 892 XXXX 1322 XXXX XXXXX -----|

Level Of Service Module: Stopped Del: 2.3 XXXX XXXXX XXXXX XXXX XXXX 4.1 XXXX 2.8 XXXXX XXXXX Shrd StpDel:xxxxx xxxx xxxxx xxxxx xxxxx xxxxx 3.3 xxxxx xxxxx xxxxx Shared LOS: * * * * * * * * * * * * * 0.0 3.2 0.0 ApproachDel: 2.0

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Thu Aug 20, 1998 14:08:40 SMFTAM2.CMD

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Daybreak Mine

Future (1999) Plus Project Traffic Volumes - no conveyor AM Peak Hour

-----Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) ************************** Intersection #11 Daybreak/Hyatt/269th *********************** Average Delay (sec/veh): 1.5 Worst Case Level Of Service: A ***************** North Bound South Bound East Bound West Bound Approach: L-T-R L-T-R L-T-R Movement: Uncontrolled Uncontrolled Stop Sign Stop Sign Control: Include Include Include Include Rights: 0 1 0 0 0 0 0 0 1 0 0 0 1! 0 0 0 0 0 0 Lanes: Volume Module: 87 Base Vol: 43 34 0 0 201 2 0 2 2 2 0 89 0 0 Initial Bse: 44 35 0 0 205 0 0 0 0 0 0 n Added Vol: 0 0 ٥ PasserByVol: -1 0 0 Initial Fut: 43 35 0 0 0 0 0 0 0 9.9 2 2 0 0 205 2 2 0 98 0 0 Ω PHF Volume: 47 38 0 0 225 0 0 0 Ω 0 0 O 0 0 0 0 Reduct Vol: ٥ Final Vol.: 47 38 0 0 225 2 Λ 0 98 ٥ Adjusted Volume Module: -44 Grade: +4% 0.00 0.45 xxxx xxxx 0.00 0.96 0.00 0.55 0.04 0.00 0.55 0.00 % Cycle/Cars: 0.00 0.51 * Truck/Comb: 0.49 0.00 0.30 0.80 0.50 1.00 xxxx xxxx Cvcl/Car PCE: 0.70 1.40 XXXX XXXX Trck/Cmb PCE: 3.00 6.00 1.50 2.00 1.00 1.20 0 0 0 0 225 2 3 0 124 Adj Vol.: 103 38 0 Critical Gap Module: MoveUp Time: 2.1 xxxx xxxxx xxxxx xxxx 3.4 xxxx 2.6 xxxxx xxxx xxxx Critical Gp: 5.0 XXXX XXXXX XXXXX XXXX XXXXX 6.5 XXXX 5.5 XXXXX XXXXX Capacity Module: Cnflict Vol: 228 XXXX XXXXX XXXX XXXX XXXX 312 XXXX 226 XXXX XXXX XXXX Potent Cap.: 1336 XXXX XXXXX XXXX XXXX XXXXX 699 XXXX 1063 XXXX XXXXX Adj Cap: 1.00 xxxx xxxxx xxxx xxxx xxxxx 0.92 xxxx 1.00 xxxx xxxx xxxxx Move Cap.: 1336 XXXX XXXXX XXXX XXXX XXXX 644 XXXX 1063 XXXX XXXX XXXX Level Of Service Module: Stopped Del: 2.8 xxxx xxxxx xxxxx xxxx 5.6 xxxx 3.7 xxxxx xxxx xxxxx LOS by Move: A * * * * * * * * * Movement: LT - LTR - RT Shrd StpDel:xxxxx xxxx xxxxx xxxxx xxxxx xxxxx 3.8 xxxxx xxxxx xxxxx xxxxx Shared LOS: * * * * * * * A * * * * 0.0 3.8 ApproachDel:

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08/20/1998 14:34

ApproachDel:

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SMFTPM1.CMD

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Davbreak Mine Future (1999) Plus Project Traffic Volumes - with conveyor PM Peak Hour

Impact Analysis Report Level Of Service

Thu Aug 20, 1998 14:09:11

Intersection	Base		Puture	Change
211002000000	Del/ '	V/	Del/ V/	in
	LOS Veh	c Los	Veh C	
# 2 Moore/Bevin/284th	A 0.3 0.0	00 A	0.3 0.000	+ 0.000 V/C
# 9 61st/Bennet/Main Access	A 1.4 0.0	00 A	1.6 0.000	+ 0.000 V/C
# 11 Daybreak/Hyatt/269th	A 0.6 0.0	00 A	0.6 0.000	+ 0.000 V/C
# 13 #2nd Ave/279th	в 0.70.0	00 B	0.7 0.000	+ 0.000 V/C

Thu Aug 20, 1998 14:09:11 SMFTPM1.CMD Davbreak Mine Puture (1999) Plus Project Traffic Volumes - with conveyor PM Peak Hour Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative) ************************** Intersection #2 Moore/Bevin/284th ********************** Average Delay (sec/veh): 0.3 Worst Case Level Of Service: ************************ North Bound South Bound East Bound Approach: L-T-R L-T-R L-T-R Movement: Stop Sign Stop Sign Uncontrolled Uncontrolled Control: Include Include Include Include Rights: 0 0 1! 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0 0 0 Lanes: .|-----||------| ------Volume Module: 0 0 0 O 3 12 0 29 Base Vol: 0 0 0 1 3 3 12 0 Initial Bse: 0 30 5 0 0 0 ٥ Added Vol: 0 0 0 1 ٥ O ٥ 0 PassarBvVol: 0 1 0 3 13 0 n 0 1 0 31 0 5 Initial Fut: PHF Adi: 0 0 0 PHF Volume: 0 39 7 4 17 0 0 n ٥ 0 0 Reduct Vol: 0 0 0 0 4 17 0 0 0 ٥ Final Vol.: 0 39 7 Adjusted Volume Module: 0% Grade: 0% XXXX XXXX XXXX XXXX % Cycle/Cars: 0.00 0.97 0.00 0.97 XXXX XXXX * Truck/Comb: 0.03 0.00 0.03 0.00 xxxx xxxx XXXX XXXX Cycl/Car PCE: 0.50 1.00 0.50 1.00 XXXX XXXX XXXX XXXX 1.50 2.00 Trck/Cmb PCE: 1.50 2.00 1 0 4 0 0 0 4 17 0 0 39 7 Adi Vol.: Critical Gap Module: MoveUp Time:xxxxx xxxx xxxxx 2.1 xxxx xxxxx xxxxx xxxxx 3.4 xxxx 2.6 Critical Gp:xxxxx xxxx xxxxx 5.0 xxxx xxxxx xxxxx xxxxx 6.5 xxxx 5.5 Capacity Module: Potent Cap.: xxxx xxxx xxxxx 1630 xxxx xxxxx xxxx xxxx xxxxx 973 xxxx 1318 Adj Cap: XXXX XXXXX 1.00 XXXX XXXXX XXXX XXXXX 1.00 XXXX 1.00 Move Cap.: XXXX XXXX XXXXX 1630 XXXX XXXXX XXXX XXXX 971 XXXX 1318 Level Of Service Module: Stopped Del:xxxxx xxxx xxxxx 2.2 xxxx xxxxx xxxxx xxxxx 3.7 xxxx 2.7 LOS by Move: * * * A * * * * . * * Movement: LT - LTR - RT LT - LTR - RT LT - LTR - RT * * * * A * Shared LOS: * * * * * *

Filename: SMFTPM1.OUT

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0.0

08/20/1998 14:34

Level Of Service Module:

0.3

ApproachDel:

SMFTPM1.CMD

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5.0

Daybreak Mine

Puture (1999) Plus Project Traffic Volumes - with conveyor PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

************************* Intersection #13 82nd Ave/279th ***************** Worst Case Level Of Service: В ^ 7

Average Dela	y (sec/veh	ı):	0.7	Wo		e Level Of	Service:	
*******	*****	*****	****	******			West B	
Approach:	North E			Bound		t Bound T - R	L - T	
Movement:	L - T	~ R	· r - ,	T - R	, L	T - K		
					1	- 64	Stop S	dan
Control:	Unconti			trolled	800	nclude	Incl	1100
Rights:		ude		clude		1! 0 0	0 0 11	
Lanes:	0 0 1	. 0 0 .	, 0 0	0 1 0	1 0	11 0 0		
Panes:							11	•
Volume Modul			_	56 2	1	3 11	11 5	5
Base Vol:	28 185		-		_	-		
Growth Adj:		1.02	1.02 1.	57 2	1.02 1	3 11	11 5	
Initial Bse:			0	0 0	ō	-	0 0	
Added Vol:	•		0	0 0	Õ	•	0 0	0
PasserByVol:			-	57 2	ĭ	•	11 5	5
Initial Fut:			1.00 1.	<i>-</i>	1.00 1			1.00
User Adj:			0.85 0.		0.85		0.85 0.85	0.85
PHF Adj:			0.55 0.		1	4 13	13 6	6
PHF Volume:			_	0 0	-	0 0	0 0	0
**********		28	0	67 2	ĭ	4 13	13 6	6
Final Vol.:			. •	-	_	-		
Adjusted Vol	ume Module			0%		0%	01	•
Grade: % Cycle/Cars				0.92	0.0	0 0.97	XXXX	XXXX
* Truck/Comb		0.00		0.00	0.0	3 0.00	XXXX	
PCE Adi:	•			00 1.00	XXXX X	XXXX XXXX	1.10 1.10	1.10
Cycl/Car PCE		1.00		1.00	0.5	0 1.00	XXXX	XXXX
Trek/Cmb PCE	1.50	2.00		2.00	1.5	0 2.00	XXXX	
Adj Vol.:		28		67 2	1	4 13	15 7	7
Critical Gan	Module:							
MoveUp Time:	2.1 XXX	xxxxx	xxxxx xx	xx xxxx	3.4	3.3 2.6		2.6
and admin and	E A YYY	TYYYY	XXXXX XX	XXXXX XX	6.5	6.U S.S		
CLIFICAL OF:								
Capacity Mod	ule:							
Cnflict Vol:	70 xxx	xxxxx x	XXXX XX	XXXXX XX	345	353 68		
Potent Cap. :	1588 xxx	XXXXX	XXXX XX	XXXXX XX	668	712 1278		
					0 97 (97 1.00	0.97 0.97	7 1.00

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0.0

Adj Cap: 1.00 XXXX XXXXX XXXX XXXX XXXXX 0.97 0.97 1.00 0.97 0.97 1.00 Move Cap.: 1588 XXXX XXXXX XXXX XXXX XXXX 647 694 1278 644 705 1050

Stopped Del: 2.3 xxxx xxxxx xxxxx xxxx xxxxx 5.6 5.2 2.8 5.7 5.1 3.4 Shrd StpDel:xxxxx xxxxx xxxxx xxxxx xxxxx xxxxx 3.5 xxxxx xxxxx 5.1 xxxxx Shared LOS: * * * * * * * * A * * B *

Filename: SMFTPM1.OUT

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Movement:

Adjusted Volume Module:

L-T-R L-T-R L-T-R

|-----|

L - T - R

Daybreak Mine

Future (1999)Plus Project Traffic Volumes - no conveyor PM Peak Hour

Level Of Service Computation Report

1994 HCM Unsignalized Method (Future Volume Alternative)

Intersection	#9 61st/Bennet/	Main Access	*****	******
Sucreme Delas	/ (sec/yeh):	1.7	Worst Case Level Of	Service: A
Approach:	North Bound	South Bound	East Bound	West Bound

Control: Rights:	Un	contro Incl		Un	Uncontrolled Include			Stop Sign Include			stop sign Include		
Lanes:	0 :	1 0	0 0	0 (0 0	1 0	0 0	1!	0 0	0 (0 0	0 0	
Volume Modul	9: 11	23	•		14	, 4	' 6	0	24		0	0	
Base Vol: Growth Adj:	1.00	1.02	1.00	1.00	1.02	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
Initial Bse: Added Vol:	11 0	23	0	0	14 0	0	Ö,	0	24 0	Ö	0	0	
PasserByVol: Initial Fut:	4 15	0 23	0	0	0 14	7 11	10 16	0	9 33	0	0	0	
User Adj:	1.00	1.00			1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	
PHF Adj: PHF Volume:	0.81	0.81 29	0.81 0	0.81	18	14	20	0	41	0	0	0	
Reduct Vol: Final Vol.:	0 19	-	0	0	0 18	0 14	0 20	0	41	0	0	0	

Grade:	0%	0%	0%	0%
	0.00 0.85	XXXX XXXX	0.00 0.68	XXXX XXXX
* Truck/Comb:		XXXX XXXX	0.32 0.00	XXXX XXXX
PCE Adj:		1.10 1.00 1.00	XXXX XXXX XXXXX	1.10 1.10 1.10
Cycl/Car PCE:	0.50 1.00	XXXX XXXX	0.50 1.00	XXXX XXXX
Trck/Cmb PCE:	1.50 2.00	XXXX XXXX	1.50 2.00	0 0 0
Adi Vol.:	20 29 0	0 18 14	23 0 47	0 0 0

Critical Gap Module: MoveUp Time: 2.1 XXXX XXXXX XXXXX XXXX 3.4 XXXX 2.6 XXXXX XXXX Critical Gp: 5.0 XXXX XXXXX XXXXX XXXX 6.5 XXXX 5.5 XXXXX XXXX

Capacity Module: Potent Cap.: 1657 XXXX XXXXX XXXX XXXX 962 XXXX 1346 XXXX XXXX Adj Cap: 1.00 xxxx xxxxx xxxx xxxx xxxxx 0.99 xxxx 1.00 xxxx xxxx xxxxx Move Cap.: 1657 XXXX XXXXX XXXX XXXX XXXX 950 XXXX 1346 XXXX XXXX XXXX ------

Level Of Service Module: Stopped Del: 2.2 xxxx xxxxx xxxxx xxxx xxxx 3.9 xxxx 2.8 xxxxx xxxx xxxxx LOS by Nove: A * * * * * * * * * * Movement: LT - LTR - RT

* * Shared LOS: * * * * * * * A 0.0 3.1 ApproachDel: 0.9 0.0

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Thu Aug 20, 1998 14:09:42 SMPTPM2.CMD

Davbreak Mine

Future (1999) Plus Project Traffic Volumes - no conveyor PM Peak Hour

Level Of Service Computation Report 1994 HCM Unsignalized Method (Future Volume Alternative)

Filename: SMFTPM2.OUT

********	****	14***	******	tt/269	th ****	*****	*****	****	*****	*****	****	****
Average Delay	(sec	c/veh)	:	0.6		Wo	rst Ca	se Le	vel Of	Servi	.ce :	A
*******						*****					st Bo	_
Approach:		rth_Bo			ith_Bo			st Bo T			T	
Movement:	L .	- T	- R	. L -	T	- R	, L	1	- K	- <u>u</u>		
						1		04		-	op Si	an l
Control:	Unc	contro				olled			gn		Incl	
Rights:		Inclu	ide		Inclu			Inclu	0 0			0 0
Lanes:	0 1	LO	0 0	. 0 (0	1 0	ָ ט ט					
										1		1
Volume Module				_					22	0	0	0
Base Vol:	45		0	0	87	1	1	0	1.02	1.02	-	1.02
		1.02	1.02	1.02		1.02	1.02		22	1.02	1.02	0
Initial Bse:	46	257	0	0	89	1	1	0	22	0	0	0
Added Vol:	0	0	0	0	0	0	0	0	8	0	0	Ö
PasserByVol:		0	0	0	0	0	1	0	-	0	0	ő
Initial Fut:	50		0	0	89	1	2	0	30	1.00	-	1.00
User Adj:		1.00	1.00	1.00		1.00	1.00		1.00	0.86		0.86
PHF Adj:		0.86	0.86	0.86		0.86	0.86		0.86		0.86	0.86
PHF Volume:	58	299	0	0	103	1	2	0	35	0	0	0
Reduct Vol:	0	0	0		0	0	0	0	0	0	0	0
Final Vol.:	58	299	0	0	103	1	2	0	35	U	U	v
Adjusted Volu	ıme Mo		:								0%	
Grade:		+4%			-44		_	0%				
* Cycle/Cars:		.00 (.00			00 0				CXXX
* Truck/Comb:		.04 (0.00			0.00			cccx
PCE Adj:	XXXX	1.00	1.00			1.00			xxxxx		1.10	
Cycl/Car PCE:		.70			.30 (00			CXXX
Trck/Cmb PCE:	3	.00 6	5.00			1.20	1.	50 2	.00		CXX 2	cxxx
Adj Vol.:	85		0					_				
		299	U	0	103	1	3	0	38		0	0
Critical Gap	Modu:	le:		_		_		-		0		
Critical Gap MoveUp Time:	Modu:	le:	xxxx	xxxx	xxxx	xxxx	3.4	xxxx	2.6	0 xxxxx	xxxx	xxxxx
MoveUp Time:	Modu:	le: xxxx	xxxxx	XXXXX	XXXX	xxxxx	3.4	XXXX	2.6 5.5	0 xxxxx xxxxx	xxxx	xxxxx
MoveUp Time:	Modu:	le: xxxx	xxxxx	XXXXX	XXXX	xxxxx	3.4	XXXX	2.6 5.5	0 xxxxx xxxxx	xxxx	xxxxx
MoveUp Time: Critical Gp: Capacity Modu	Modu: 2.1 5.0	le: xxxx xxxx	xxxxx	xxxxx 	xxxx xxxx	xxxxx xxxxx 	3.4 6.5	xxxx	2.6 5.5	0 XXXXX XXXXX	xxxx	xxxxx xxxxx
MoveUp Time: Critical Gp:	Modu: 2.1 5.0	le: xxxx xxxx	xxxxx	***** ***** 	xxxx	****** ******	3.4 6.5 	xxxx xxxx	2.6 5.5 	xxxxx xxxxx 	xxxx	xxxxx xxxxx
MoveUp Time: Critical Gp: Capacity Modu	Modu: 2.1 5.0 11e: 104 1529	le: xxxx xxxx xxxx	xxxxx xxxxx xxxxx	xxxx 	XXXX XXXX XXXX	******* ******************************	3.4 6.5 461 573	xxxx xxxx xxxx	2.6 5.5 104 1227	0 xxxxx xxxxx 	xxxx xxxx	xxxxx xxxxx xxxxx
MoveUp Time: Critical Gp: 	Modu: 2.1 5.0 1e: 104 1529 1.00	le: xxxx xxxx xxxx xxxx xxxx	XXXXX	XXXX XXXX XXXX	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93	XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00	XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: 	Modu: 2.1 5.0 1e: 104 1529 1.00	xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX	XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534	XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227	XXXX XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: Capacity Modu Cnflict Vol: Potent Cap: Adj Cap: Move Cap:	Modu: 2.1 5.0 1le: 104 1529 1.00 1529	xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX XXXXX	XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534	XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227	XXXX XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: 	Modu: 2.1 5.0 1le: 104 1529 1.00 1529 	xxxx xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX XXXXX	XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534	XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227	0 xxxx xxxx xxxx xxxx xxxx	XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: Capacity Modu Cnflict Vol: Potent Cap.: Adj Cap: Move Cap.:	Modu: 2.1 5.0 16: 104 1529 1.00 1529	xxxx xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX XXXXX	XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534	XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227	XXXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: Capacity Modu Cnflict Vol: Potent Cap: Adj Cap: Move Cap: Level Of Serv Stopped Del:	Modul 2.1 5.0 104 1529 1.00 1529	xxxx xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX	XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534 	XXXX XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227 3.0	0 XXXXX XXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: 	Modu. 2.1 5.0 104 1529 1.00 1529 	xxxx xxxx xxxx xxxx xxxx xxxx xxxx xxxx xxxx	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX	XXXXX XXXXX XXXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX XXXX	3.4 6.5 461 573 0.93 534 6.8	XXXX XXXX XXXX XXXX XXXX XXXX	2.6 5.5 104 1227 1.00 1227 	XXXXX XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX
MoveUp Time: Critical Gp: Capacity Modu Cnflict Vol: Potent Cap: Adj Cap: Move Cap: Level Of Serv Stopped Del: LOS by Move: Movement: Shared Cap:	Modu: 2.1 5.0 104 1529 1.00 1529 	XXXX XXXX XXXX XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX XXXX	XXXXX XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534 6.8 LT -	XXXX XXXX XXXX XXXX XXXX LTR 1135	2.6 5.5 104 1227 1.00 1227 3.0 *	O XXXXX XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX LTR	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX XXXX
MoveUp Time: Critical Gp: Capacity Modu Cnflict Vol: Potent Cap: Adj Cap: Move Cap: Level Of Serv Stopped Del: LOS by Move:	Modu: 2.1 5.0 104 1529 1.00 1529 7ice 2.4 A LT xxxx	XXXX XXXX XXXX XXXX XXXX XXXX XXXX LTR XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX - RT XXXXX XXXXX	XXXXX XXXXX XXXX XXXX XXXX XXXXX XXXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX	3.4 6.5 461 573 0.93 534 6.8 LT - XXXX	XXXX XXXX XXXX XXXX XXXX LTR 1135	2.6 5.5 104 1227 1.00 1227 	O XXXXX XXXXX XXXX XXXX XXXX XXXX	XXXX XXXX XXXX XXXX XXXX XXXX LTR	XXXXX XXXXX XXXXX XXXXX XXXXX XXXXX XXXX

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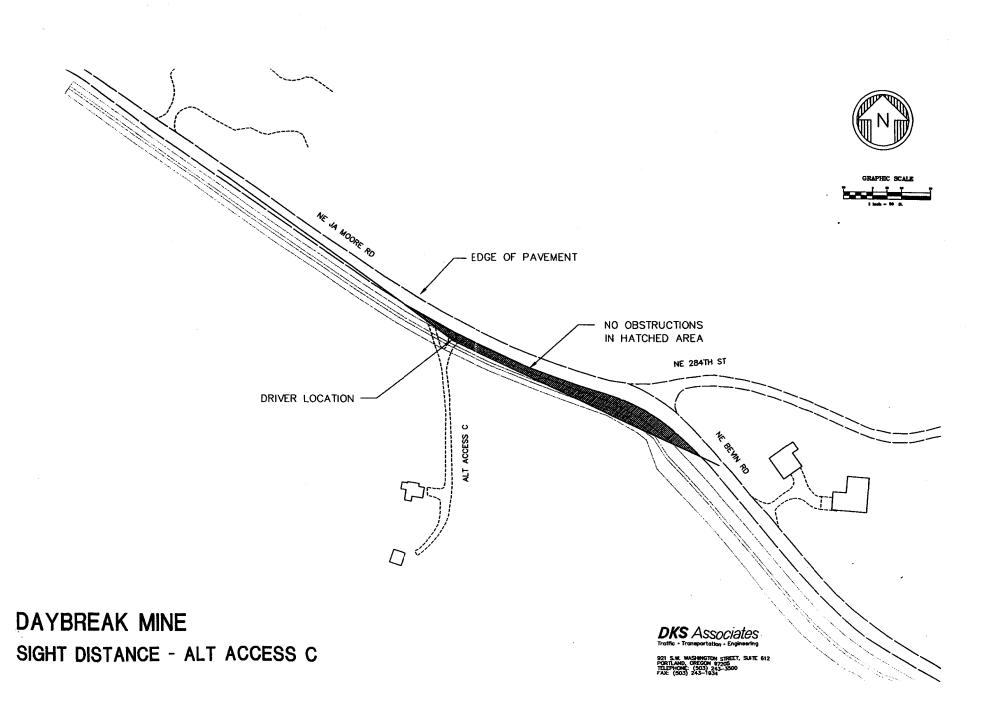
A *

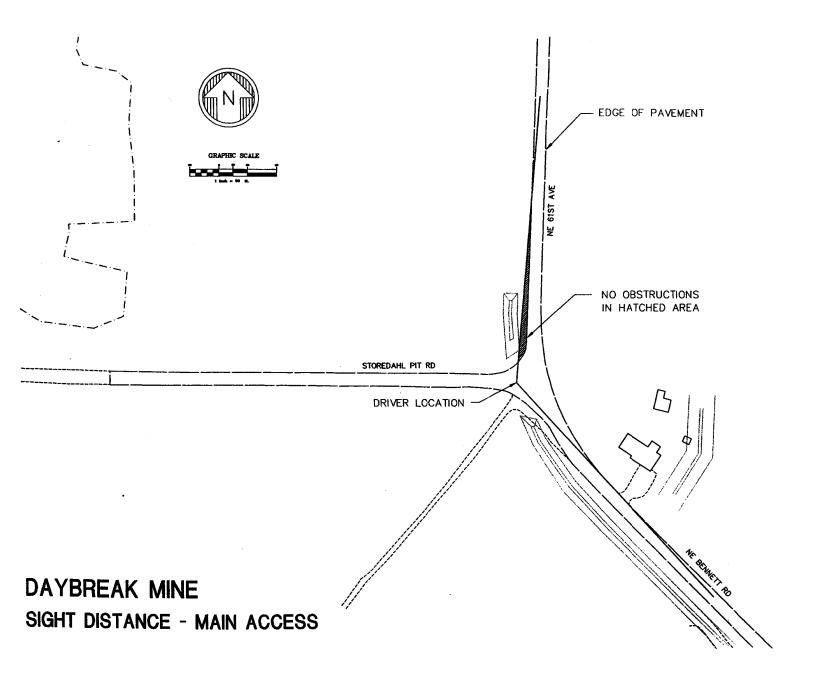
Shared LOS: * * * * * * *

ApproachDel:

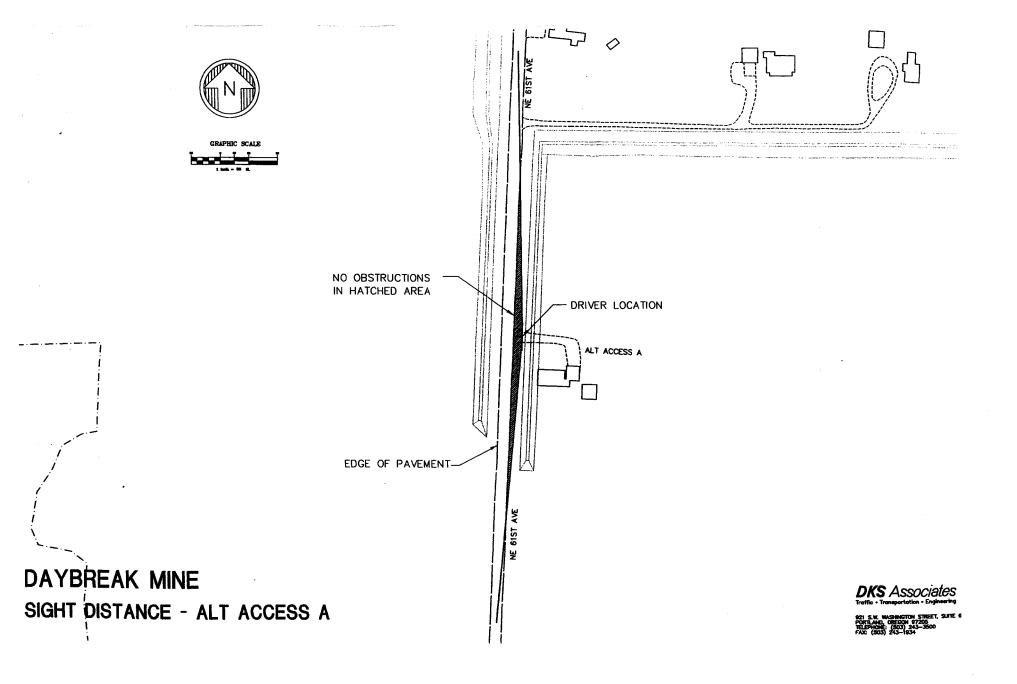
Appendix D

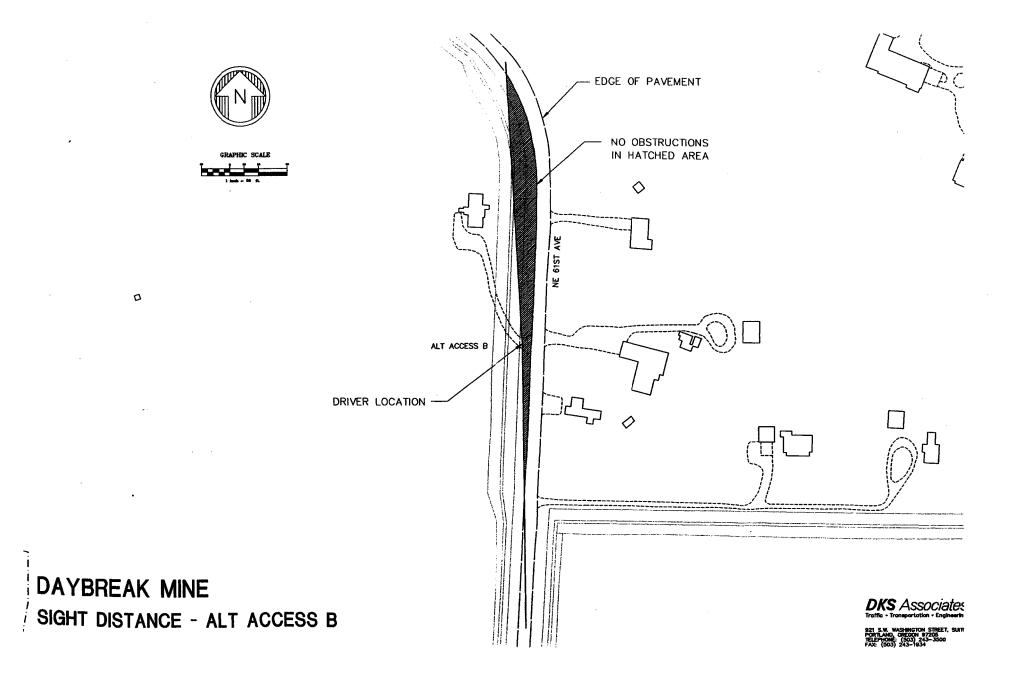
Access Sight Distance











Appendix E

Accident Rate Calculations

Accident Rate Calculations

ADT Estimations

Use 24-hour tube count at Bennet Road Near Storedahl Pit Road to determine relationship between pm peak volumes and daily volumes:

Bennet Road s/o Storedahl

PM Peak Hr Volume 115 Daily Volume 1453

Percentage 7.91% Apply this percentage to all PM peak counts to estimate ADT at each intersection

Intersection	PM pk vol	ADT	Accidents* Ac	c Rate**
NE JA Moore Rd/NE 284th St	53	670	1	0.82
NE 61st Ave/Bennet Rd	82	1036	0	0.00
NE Hyatt Rd/NE Daybreak Rd	408	5155	0	0.00
NE 82nd Ave/NE 279th St	330	4169	3	0.39

Accidents from 1992-1996 (5 years). Obtained from Clark County Public Works.

^{**} Accident rate calculation per ITE Traffic Engineering Handbook

Appendix F

Trip Generation Data/Calculations

Daybreak Mine

Existing Trip Generation

TRUCKS			EMPLOYEES	
Export (tons/day)	4,000		AM trips in	O
Export (30-ton loads/day)	113		AM trips out	0
Export (8-yd loads/day)	58		PM trips in	3
Export (loads/day)	171	174	PM trips out	10
Import (tons/day)	5,000		-	
Import (loads/day)	167	132	•	
Total (loads/day)	338	306		
ACTUAL TRAFFIC COUNTS			ADJUSTED TRAFFIC	COUNTS
AM in	41		AM in	45
AM out	38		AM out	42
PM in	14		PM in	15
PM out	27		PM out	30

^{*}Proposed trip generation numbers were based on the numbers shown above and factored up to represent proposed levels of operation.



July 21, 1998

Mr. Brian Copeland, P.E. DKS Associates 921 SW Washington Street Suite 612 Portland, OR 97205

Re:

Daybreak Mine

Dear Brian:

This letter revises the information presented in my June 19 letter regarding traffic and transportation data and projections associated with the Daybreak Mining and Habitat Enhancement Project.

- Presently, export volumes average approximately 4,000 tons of aggregate per day between June and November and 1,500 tons per day the remainder of the year. Import volumes presently average approximately 4,500 tons per day during 8-hour shifts and a fleet of 6 trucks dedicated to round trip hauls; peak day volumes average approximately 5,000 tons which requires a 10-hour shift and typically uses 7 trucks. Future imports, as previously stated, will be reduced by approximately 50 percent. All hauling conducted by Storedahl is with 30-ton trucks.
- Activities to be conducted on site include mining, processing, sorting and stockpiling sand and gravel. The preferred method of moving raw materials from an active pit to the processing area continues to be by conveyor. However, failure to acquire the necessary permits to extend the conveyor system would necessitate hauling the raw material to the processing area by truck via NE 61st Avenue. Average daily volume of hauled raw material would be approximately 2,500 tons and peak days would see approximately 4,000 tons moved. All raw material hauling would be by 30-ton trucks. Access to the county road would be from existing driveways only. On-site truck haul routes would be limited to that stretch of county road from the active driveway access to Storedahl Pit Road.
- Cash sales presently account for approximately 15 percent of total export volume. The average load is approximately 8 tons per transaction. Future cash sales will be restricted to operating hours after 9:00

I hope this information clarifies the intent of the project. If you need additional information or have any questions, please call me.

Very trally yours,

Skip Urling, AICP

Co:

Kimball Storedahl Randy Sweet JUL 2 2 1998 DKS-PORTLAND June 19, 1998

Mr. Brian K. Copeland, P.E. DKS Associates 921 SW Washington Street Suite 612 Portland, OR 97205

Re: Daybreak Mine Transportation Study Data Needs

Dear Brian:

The following information is in response to your June 16 fax outlining the data needs for the transportation study to support the development permits for the Daybreak Mine and Habitat Enhancement Project.

- 1. Once permitted, the projected volume of material imported to the site for processing is 2,500 tons per day. This material will be brought to the Daybreak site only between March and November, and will be transported in trucks with a 30-ton capacity. The projected export is 5,000 tons per average annual day. Peak operations will result in 8,000 tons per day being exported between June and October, and 3,000 tons per day between November and May. Operations will occur Monday through Saturday year round.
- Presently, the average export is 4,000 tons per day between June and November and 1,500 tons per day the remainder of the year. Import volumes are between 5,000 and 6,000 tons per day between March and November. All import and export hauling is with 30-ton trucks.
- 3. The best we can do on historic activity is volume of material sold from Daybreak.

Year	Tons Sold
1988	152,101
1989	37,952
1990	562,508
199 1	557,338
1992	134,301
1993	80,023
1994	58,846
1995	57,096
1996	76,457
1997	367,682
1998	184,593 (thru May)

4. Projected Employees:

Monday-Friday, 7:00 am to 5:30 pm: 10 employees

Mr. Brian Copeland, P.E. Daybreak Mine—Traffic Study Data Needs June 19, 1998 Page 2

6:00 pm to 2:30 am:

3 employees

Saturday

7:00 am to 3:30 pm:

3 employees

6:00 am to 2:30 pm:

2 employees

5. Current Employees: Same as above.

6. Hours of Operation: See Item 4.

- 7. On-site activities: Activities to be conducted on site include mining, processing, sorting and stockpiling sand and gravel. The preferred alternative for delivering the mined material to the processing area is by conveyor. However, you should analyze the effects of trucking the material from the pits to the processing area via J.A. Moore Road /NE 61st Avenue. Average -daily volumes will be 2,500 tons transported in 30-ton trucks. All on-site haul traffic would be routed through four access points in series, as the area of active mining shifts. Please see the attached site plan for approximate access points.
- 8. Typical truck routes are highlighted on the attached vicinity maps, with haul distributions noted.
- 9. The only access to the processing area is Storedahl Pit Road. <
- 10. Other issues.

1. Cash sales account for about 15 percent of the total volume leaving the site. The size of

the haul trucks for these private sales vary.

2. The residents along Manley Road, which is the route to the Tebo pit, the current source of imported raw rock, have serious concerns about the truck traffic associated with that import hauling. Stress that permitting the Daybreak site will reduce Storedahl's import hauling from the Tebo pit by 50 percent.

If you need additional data or have any questions, please call me at your earliest convenience.

Very truly-yours,

kjo Urling, AICP

Enclosures

APPENDIX B

Noise Impact Assessment for the Expansion of the Daybreak Mine Excavation Area

Clark County Washington

To: J.L. Storedahl & Sons 2233 Talley Way Kelso, WA 98626

NOISE IMPACT ASSESSMENT FOR THE EXPANSION OF THE DAYBREAK MINE EXCAVATION AREA CLARK COUNTY, WASHINGTON

DSA File: 159916

Attn: Kimball Storedahl

Prepared By: Daly-Standlee & Associates, Inc.

Kerrie G. Standlee, P.E.

August 22, 2000

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1.0 INTRODUCTION

J.L. Storedahl & Sons, Inc. proposes to extend the excavation area at the Daybreak mine located on the East Fork of the Lewis River in Clark County, Washington (see Figure 1). The Clark County Department of Community Development determined that an Environmental Impact Statement (EIS) is required for the proposed action and in preparation for writing of the EIS, J.L. Storedahl & Sons, Inc. asked Daly-Standlee & Associates, Inc. (DSA) to perform a Noise Impact Assessment for the planned expansion.

This report presents the information used by Daly-Standlee & Associates, Inc. in the noise impact assessment. The information includes a description of the proposed extraction operations at the mining site, a discussion relative to the noise descriptors used in the analysis, a discussion about the existing environment at noise sensitive properties around the mining site and a discussion about the future noise environment expected at noise sensitive properties around the mining site. Finally, the report presents a comparison of the expected future acoustical environment at noise sensitive properties around the mining operations with appropriate standards set by governmental agencies and to the existing environment to determine noise impacts.

2.0 EXECUTIVE SUMMARY

J.L. Storedahl and Sons, Inc. proposes to extend the excavation area at the Daybreak mine site located on the East Fork of the Lewis River. Currently, raw aggregate materials are trucked to the Daybreak site and crushed and screened at the plant located on the site and crushed materials generated at the Daybreak site are trucked off-site for distribution to the public. J.L.Storedahl & Sons, Inc. plans to continue crushing aggregate materials at the Daybreak site and the company proposes to extend the aggregate extraction area at the Daybreak site to supply the crushing and screening plant.

Noise impacts were assessed at 17 residential properties located around the mining site. The 17 properties were considered to represent the noise sensitive properties where there was the most potential for noise impacts from the proposed expansion. Ambient sound levels were measured at 9 locations near several of the residential properties to provide a baseline for the impact analysis. Measurements were made of the sound levels radiating from the equipment expected to operate at the facility. The equipment sound data was included in computer models to predict the future sound levels at the 17 residential properties around the mining site. The predicted future sound levels were compared with the existing sound levels at the residential properties and with appropriate government criteria to determine noise impacts.

The results of the noise study indicate the crushing operation at the Daybreak pit will generate no additional impact on any of the residential properties around the site. There are no plans to move the crushing operation from its historic location, and there should be no change in the crushing operation noise reaching any residence.

The results of the noise study indicate the extension of the mining area at the Daybreak pit will generate no significant impacts on the residences south of the East Fork Lewis River because the properties are to far from the noise sources. However, the results indicate there will be significant

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The results of the noise study indicate the extension of the mining area at the Daybreak pit will generate no significant impacts on the residences south of the East Fork Lewis River because the properties are to far from the noise sources. However, the results indicate there will be significant

noise impacts at various properties north of the East Fork Lewis River if noise mitigation measures are not included in the mining plan. The results indicate that during Phases 1 through 4 (shown in Figure 2), the loudest hour statistical noise levels at residential properties at or near modeling locations 1, 2, 5, 6, 7, 8, 9, 10 and 11 will exceed the WAC noise limits if mitigation measures are not implemented. Noise levels at the 9 locations will also exceed the Clark County SEPA criteria if mitigation measures are not used during mining in the different phases.

Mitigation measures which can be used to reduce noise impacts to "insignificant" at all residences around the site include the construction of berms or engineered barriers at the locations shown in Figure 3 and at the heights and lengths presented in Table 5 of this report. The times when the berms or barriers are required are discussed in detail in Section 11.0 of the report.

Truck traffic to and from the site was found to have no impact on the residential property north or south of the East Fork Lewis River because extension the mining area will not change the truck traffic already traveling to and from the site.

3.0 OVERVIEW OF THE NOISE IMPACT ASSESSMENT PROCEDURE

In conducting the noise impact assessment, the following steps were taken:

- 1. The existing noise environment was monitored at 9 residential properties around the mining areas to gather information on the type of noise sources currently influencing environment at the residential properties and to provide a noise level baseline for the impact analysis. The data was used to verify the accuracy of the noise model used to predict future noise levels.
- 2. Future noise levels at residential properties around the mine site were predicted for the conditions that would be present during the expansion of the excavation area.
- 3. The future noise levels predicted at the residences were compared with government standards and to the existing environment at the residences to determine if negative noise impacts would occur.
- 4. If significant noise impacts were found, noise mitigation measures were identified.

To fully predict the future noise levels that would be generated during excavation operations in the proposed excavation area, a noise model was developed in which noise was predicted from each of three groups of sound sources: the existing crushing operation, the proposed excavation operation and off-site truck traffic. The sound levels generated by the three source groups were predicted utilizing computer programs that include the effects of atmospheric absorption on sound propagation in the environment. Reference sound data for the analysis was obtained from measurements made by Daly-Standlee & Associates, Inc. and from data supplied by equipment manufacturers. Sound data for the existing crushing equipment and haul trucks was measured by Daly-Standlee & Associates, Inc. Sound data for the excavation equipment was supplied by the manufacturer for the excavation equipment owned by J.L. Storedahl & Sons, Inc.

Three criteria were used to assess noise impacts associated with the proposed excavation operations; 1) Chapter 173-60, "Maximum Environmental Noise Levels", of the Washington Administrative Code

(WAC), 2) Chapter 20.50.025(3)(g) of the Clark County Code and 3) a subjective criteria developed through the use of people's perceptions of noise and the general guidelines about noise perception established by the U.S. Environmental Protection Agency. The WAC criteria and the Clark County Code were used in an attempt to assess the maximum sound level expected to radiate from the proposed operation. The subjective criteria was used to evaluate the change in noise level expected with the proposed operations.

In using the "maximum level" criteria, the noise radiating to residences from the mining activities was compared with the maximum noise levels allowed to radiate by WAC 173-60-040, "Maximum Permissible Environmental Noise Levels" and the Clark County Code Chapter 20.50.025(3)(g). If the mining noise radiating to a residential property exceeded the maximum sound levels allowed in those codes, the proposed operations were considered to have a "serious" noise impact on the residence and mitigation measures were needed to reduce the noise levels at the residence.

In using the "change in noise level" criteria, the predicted mining generated noise levels reaching residential properties were compared with the existing ambient sound levels at the residential properties to determine the change, if any, that would occur with the proposed operations. The difference between the existing noise levels and the mining and processing generated noise levels was then evaluated using the fact that, generally speaking, most people think that a 3 dB increase in sound level is just barely perceptible, a 5 dB increase in sound level is very perceptible and a 10 dB increase is considered by most people to be a doubling of the sound level. In this study, a change in environmental noise levels of 0 - 4 dB is defined as "insignificant" and no mitigation is needed, a change of 5 - 9 dB is defined as "significant" and mitigation measures might be considered if they are economically feasible, and a change of 10 dB or more is defined as "serious" and mitigation measures should be used to reduce the amount of change in noise level to less than 10 dB. This type of evaluation has been used by the Federal Highway Administration in assessing impacts from highway noise and by many State and local governments in assessing continuous noise sources such as the mining operation.

4.0 OVERVIEW OF EXISTING AND PROPOSED OPERATIONS

Currently at the Daybreak mine site, raw aggregate material is hauled in by truck from the Tebo gravel mine site and crushed and screened. The crushed gravel is then hauled by trucks from the site to customers in the County. The normal operating hours at the existing crushing and screening facility are 6:30 am to 5:00 pm. During periods when customer demand requires, crushing and screening operations may continue until 8 pm.

J.L. Storedahl & Sons, Inc. proposes to extend the excavation area at the Daybreak mine site to allow the extraction of raw aggregate materials in areas closer than the Tebo gravel mine to the processing facilities. Hours for the excavation of resource materials in the proposed expansion area will be basically the same as those used for the crushing and screening facilities.

The Daybreak mine site extraction area will be expanded in 7 phases as shown in Figure 2. Based on the most recent mining plan (the year 2000 mining plan), the proposed aggregate extraction will begin in the Phase 1A area and progress into the Phase 1B area and then into the Phase 1C area (see Figure 2). In these areas, because of their small size, aggregated material will likely be excavated with an excavator and loaded directly into haul trucks that will transport the material to the existing

crushing facility at the Daybreak site. Most of the aggregate extraction in these areas will very likely occur with the excavator placed near the existing grade and thus the depth of extraction in these areas will be limited to the extent of the reach from the existing grade.

Once Phases 1A, 1B and 1C are completed, a conveyor will be extended from its current terminus at the northeast corner of Pond 1to NE 61st Avenue near the approximate middle of the Phase 3 area. A trench will be dug with an excavator on the east and west side of NE 61st to allow the conveyor to be routed under NE 61st through a culvert. The material dug from the trench will be placed along the length of the trench and later placed on the conveyor during Phase 3 excavation.

On the east side of NE 61st Avenue, the trench will be continued to the east to approximately the point in Phase 3 where the eastern most reclamation island will be located. The trench will be dug to just above the water table in the Phase 3 area (approximately 12 feet below the existing grade) and the conveyor will be extended from the culvert to the end of the trench with the belting located approximately 8 feet above the floor of the trench (so that the conveyor will be located approximately 4 feet below the existing grade level). At the end of the conveyor, a feed hopper will be placed down inside the trench in preparation for receiving materials from the Phase 2 and 3 areas.

When excavation activities begin in the Phase 2A area, a front-end loader will be used to extract the resource material from the surface of the area near the northwest corner of the area and excavate down to just above the water table in that area. The material will be loaded on to haul trucks which will transport it to the feed hopper located in Phase 3. Once the front-end loader has reached the floor of the first lift (just above the water table), it will then proceed to excavate material in a southerly direction always working from the floor of the pit. After the material has been extracted down to just above the water table, an excavator will be placed down on the floor of the pit and begin to excavate the material below the water table. The excavator will begin excavation in the southeast corner of the Phase 2A area and work back northwest toward the hopper in the Phase 3 area. The excavator will extract the material from below the water table and temporarily pile it on the floor of the pit to allow water to drain. A front-end loader will then scoop the material and load it into haul trucks that will transport the material to the conveyor feed hopper in the Phase 3 area.

Because of the small size of Phase 2B and 2C areas, the resource material from those areas may only be extracted down as far as an excavator can reach from existing grades. Prior to reaching the water table, the material will be placed directly into waiting trucks which will transport the material to the conveyor feed hopper in the Phase 3 area. When excavation occurs below the water table, the resource material may temporarily be stockpiled along side the pit to allow drainage and then a frontend loader may be used to scoop the material and load it into haul trucks.

In the Phase 3 area, a front-end loader will be used to begin excavation of resource material from the surface level in the near vicinity of the conveyor feed hopper. The front-end loader will scoop material and haul it directly to the feed hopper itself without the use of haul trucks. Once a large enough area has been excavated down to just above the water table level, the front-end loader will proceed, operating from the floor of the pit, to excavate material out in all directions from the hopper toward the boundary of the Phase 3 area. After the first lift of resource material has been excavated with the front-end loader, the excavator will be placed down on the floor of the pit and begin to extract material from below the water table in the same manner described for the Phase 2A area. However, instead of the front-end loader scooping up the dewatered material and putting it into haul trucks, it will scoop up the material and transport it directly to the conveyor feed hopper. As the excavation below the water table progresses from the east end to the west end of Phase 3, the

conveyor will be retracted back to the west. Once the Phase 3 area has been fully excavated, the conveyor feed hopper will be moved to the west side of NE 61st Avenue and extended to the Phase 4 area.

Excavation in the Phase 4, 5, 6 and 7 areas will proceed as described above for the Phase 3 area. The conveyor and conveyor feed hopper will be located in a position best situated for each area prior to excavation occurring in the individual areas.

5.0 EXISTING ENVIRONMENT AROUND THE PLANNED MINING AREA

5.1 Land Use

The proposed Daybreak mine expansion area is located in central Clark County (see Figure 1 and 2). The area planned for mining is currently zoned Agricultural 20 with some Surface Mining overlay. The area north of JA Moore Rd. east of the planned mining area is zoned Rural 5. The area west of the planned Daybreak mining area is zoned Agricultural 20. The mining site is bounded on the south by land zoned Agricultural 20. The land immediately south of the historic processing plant location both along the river and on the bluff overlooking the river is zoned Agricultural 20 and Rural 5. The land south of the river near the southeast corner of the extension area is zoned Rural 5 but residential development is generally limited to the bluff overlooking the river. The land southwest of the processing plant site is zoned Agricultural 20 as far south as the bluff overlooking the river. The land on the bluff is then zoned Rural 5. A 1/2 - acre homesite along Bennett Road in the southeast area of the planned mining is zoned Agricultural 20.

5.2 Topography

The proposed mining area is located in the valley cut by the East Fork of the Lewis River. The sides of the valley have grades ranging from 4% to 25%. Above the valley, the area is generally flat except for the ravines created by the creeks which feed the E. Fk. Lewis River.

5.3 Vegetation

The north slope of the E. Fk. Lewis River valley is covered with a dense deciduous and coniferous tree forest. The south slope of the valley is covered with a dense deciduous tree forest. Above and below the valley walls, the land is farm land covered with various grasses and farm crop vegetation.

5.4 Residential Locations

Residential properties are located both on the rim of the valley and in the valley in the vicinity of the proposed mine expansion area (see Figure 2). All residential properties are currently located at least 5000 feet from the existing crushing and screening operation area at the site. Residential properties located in the valley are within 500 feet of some parts of the proposed new excavation area. Residential properties on the rim overlooking the valley will be no closer than 1000 feet from the nearest part of the proposed excavation area.

6.0 NOISE DESCRIPTORS

Sound is the term given to the physical phenomenon detected by the human ear. When physical objects are set into vibration, a minute variation is produced in the atmospheric pressure surrounding the object. The small fluctuations in the atmospheric pressure are what the ear's internal mechanism detects and in turn becomes the "music to some and noise to others".

The small fluctuation in the atmospheric pressure (sound pressure) is the physical property measured with a sound pressure level meter. Because the human ear can detect a variation in the atmospheric pressure over such a large range of magnitudes, sound pressure is expressed on a logarithmic scale in units called decibels (dB). Sound pressure level is easily measured but the subjective evaluation of the level of sound pressure by people (how people judge a sound) has been much more difficult to quantify.

Human response to sound is a function of the magnitude of a sound, the frequency spectrum of the sound (the pitch of the sound), the duration of the sound and the time when it occurs. It is difficult to describe a sound with a single number because of all these parameters that influence human response. However, over the last 20 to 25 years, there have been a significant number of studies conducted to learn more about ways to quantify sound so that there is good correlation with the human response.

Studies have shown that people are more sensitive to higher frequency sound (such as made by an air release valve) than lower frequency sound (such as made by a diesel engine). To address this preferential response to frequency, the A-weighted network was developed for sound recording instrumentation. The A-weighting network of an instrument adjusts the recorded sound pressure level in each frequency band much in the manner that the human ear responds to sound. Thus the A-weighted sound level (read as "dBA") becomes a single number that defines the level of a sound with some indication as to the human response to that sound.

The A-weighted sound level alone is not sufficient to describe the noise environment at any given location because environmental sound levels tend to constantly change with time. Therefore, an environmental noise descriptor needs to address the length of time sound is present as well as the level of the sound. One environmental noise descriptor used widely throughout the United States is the "Statistical Sound Level". The statistical sound level is generally given in terms of the level exceeded a percentage of time during a specified time period" and read " L_{xx} ". For example, the L_{50} would be that level exceeded 50% of the time during a specified time period. Usually, the specified time period is one hour in most regulations and standards.

Subjectively, an increase in sound level of 1 dBA would be judged "insignificant", an increase of 3 dBA would be "barely perceptible" by most people, and an increase of 10 dBA would generally be judged as "twice as loud".

7.0 IMPACT CRITERIA

Noise impact assessments were made in this study using the Washington State maximum noise level regulation in the Washington Administrative Code (WAC 173-60-040, see Appendix), the Clark County SEPA policy (found in Chapter 20.50.025(3)(g) of the Clark County Code) and a subjective

criteria developed through the use of people's perceptions of noise and the general guidelines about noise perception established by the U.S. Environmental Protection Agency.

The WAC 173-60-040 states that an industrial site may not radiate sound beyond the property line of a residential site that exceeds 60 dBA between the hours of 7:00 a.m. and 10:00 p.m. or 50 dBA between the hours of 10:00 p.m. and 7:00 a.m. with the exceptions that the maximum levels may be exceeded by no more than 5 dBA for fifteen minutes during any hour, by no more than 10 dBA for 5 minutes during any hour and by no more than 15 dBA for 1.5 minutes during any hour. In assessing noise impacts using the WAC noise regulation, an assessment of "serious" impact was given if the noise radiating to a residential receiver was predicted to exceed the WAC limits. An assessment of "insignificant" was assigned if the noise was predicted to be below the WAC limits.

The Washington Code is somewhat confusing and difficult to use as a criteria when it is in the form presented in the Code. To help utilize the Washington Code as a criteria, Daly-Standlee & Associates, Inc. translated the data presented in the Code into the hourly statistical sound levels shown in Table 1. The hourly statistical sound level descriptor is used as the noise descriptor of choice in noise regulations in several other states as well as cities throughout the United States and instrumentations have been made over the years that accommodate easy measurement of the descriptor.

Washington Administrative Code Noise Rules Written in Hourly Statistical Level Format for Daybreak Mine Expansion

TABLE 1

7 a.m. to 10 p.m	<u>10 p.m. to 7 a.m.</u>
$L_{25} = 60 \text{ dBA}$	$L_{25} = 50 \text{ dBA}$
$L_{08} = 65 \text{ dBA}$	$L_{08} = 55 \text{ dBA}$
$L_{03} = 70 \text{ dBA}$	$L_{03} = 60 \text{ dBA}$
$L_{\text{max}} = 75 \text{ dBA}$	$L_{\text{max}} = 65 \text{ dBA}$

Where the L_{25} , L_{08} , and L_{03} levels are those levels exceed 25%, 8% and 3% of the hour respectively.

Chapter 20.50.025(3)(g) of the Clark County code states it is the policy of the county to require the new sources of noise be limited to the maximum environmental noise levels of WAC 173-60. However, the code goes on to state that, even when the noise generated by a source will be within the limits of WAC 173-60, that increase may be considered significant if the source generates an increase in the ambient noise levels of 5 dB or more. Therefore, in this assessment, an impact of "significant" was assigned to any noise levels predicted to be more than 5 dB above the ambient noise at a receiver.

For the subjective evaluation of noise impact, an impact classification of "insignificant" was assigned to a condition where the future sound levels due to the project were 0 - 4 dBA higher than the existing sound levels. An impact classification of "significant" was assigned to conditions where the future sound levels due to the project were 5 - 9 dBA above the existing sound levels. Finally, an impact classification of "serious" was assigned to conditions where the future sound levels due to the project would be 10 dBA and more above the existing sound levels.

If a "serious" impact was determined at a receiver through any of the three criteria, mitigation

measures were concluded to be "required" to reduce noise impacts. If a "significant" impact was determined at a receiver through any of the three criteria, mitigation measures were concluded to be "required, if feasible" to reduce noise impacts. With an "insignificant" noise impact, it was concluded that no mitigation measures were required to reduce noise impact.

8.0 EXISTING NOISE ENVIRONMENT

Ambient sound levels were measured in 1991 at nine residential properties located near the proposed mining expansion area, to determine a baseline of the acoustical environment before any changes occurred at the site. The measurement locations were chosen to represent the noise-sensitive properties in different directions of the expansion area having the greatest potential of receiving noise impacts from the proposed expansion (see Figure 2).

The 1991 data was used as a baseline of the ambient acoustical environment in the noise impact analysis rather data measured during more recent periods because the original noise data were found to provide a more conservative assessment of noise impacts; thus, providing for more protection of the environment at the residences.

8.1 Measurement Locations

The 9 specific ambient noise measurement locations were chosen because they appeared to be representative of the noise sensitive properties around the expansion area that had the most potential of receiving noise impacts. The locations selected were (see Figure 2 for locations):

- 1) the Shoemaker residence (location A)
- 2) the Wiseman residence (location B)
- 3) the Foster residence (location C)
- 4) the Rose residence (location D)
- 5) the Gelfand residence (location E)
- 6) the Dorcheus residence (location F)
- 7) the Bleth residence (location G)
- 8) the Wellman residence (location H
- 9) the dairy farm on Moore Rd. north of the Daybreak site (location I)

8.2 Measurement Procedures

Community ambient sound levels were measured for one hour periods during the time periods of 6 a.m. to 8 a.m., 10 a.m. to Noon and 1 p.m. to 3 p.m. on August 12, 1991 and August 22, 1991. These time periods were chosen to provide sound data that would be representative of the ambient noise levels during morning, midday and afternoon hours of operation. During the measurement periods, significant noise sources influencing the acoustical environment at the residences were identified, including operation of the gravel plant and loading and hauling of material offsite.

The community ambient sound level measurements were made with a Larson-Davis Labs model LD-700, Type 2 Integrating Sound Level Meters programmed to take sound samples 32 times per second and determine and store hourly statistical information about the levels. The statistical data calculated by the meters corresponded to the Washington noise code, i.e., hourly L_{max} , L_{03} , L_{08} and L_{25} . In

addition to the statistical data, the meters determined the hourly $L_{\rm eq}$ sound level which is that sound level, which if present continuously for the hour, would have the same average energy as would be found for the constantly changing sound levels.

At the end of the measurement day, the data in the Larson-Davis instruments was transferred to a computer for further analysis. The print outs from the meters are presented in the appendix.

8.3 Measurement Results

Table 2 presents the average hourly statistical sound levels measured during the measurement period at each measurement position. These average sound levels are used in the impact assessment as the baseline sound levels at the residential properties. The complete results of the measurements are presented in the appendix of this report. Unless otherwise noted, the ambient sound levels presented were a result of noise generated by crickets, birds, planes, wind blowing through trees, farm machinery and roadway traffic not associated with the mining site.

Table 2
Average of Hourly Ambient Statistical Sound Levels (dBA)
From 8/12/91 through 8/22/91

Measurement Location	$\underline{\mathbf{L}}_{\max}$	<u>L</u> ₀₃	<u>L</u> ₀₈	<u>L</u> ₂₅	$\underline{\mathbf{L}}_{\mathrm{eq}}$
A	62	53 ¹	521	$\frac{L_{25}}{50^1}$	53¹
В	64	51	48	46^{1}	49
C	77^{2}	70^{2}	64^{2}	50	61
D	77^{2}	66^{2}	62^{2}	55	58
E	63	51	49	47^{1}	48
F	67	58	53	49	55
G	66	54	52	49	49
Н	67	55	53	51^{1}	51
I	75	55	49	47	50

Note: 1) Influenced by Daybreak operations.

2) Influenced by passing dump trucks to and from the Daybreak operation.

9.0 PREDICTED NOISE LEVELS

9.1 Noise Prediction Methodology

The sound sources expected at the Daybreak site were divided into three types of sources to more accurately predict the acoustical conditions expected during the continued mining of the site. The three sound sources used in the prediction were 1) the crushing related equipment, 2) excavation related equipment and 3) truck traffic. Predictions were made of the amount of noise that would reach 17 residences around the Daybreak mine site if expansion of the mining area was allowed. The effect of topography and vegetation were included in the predictions where applicable.

The results of the predictions for the three source types were combined into a final, overall sound level at each receiver. The following sections will discuss the methods and assumptions used to predict future levels and present the predicted future sound levels.

9.2 Prediction Models

A computer program was used to predict the noise levels that will radiate from the processing and excavation equipment to residences around the new mining area. The program was developed inhouse by Daly-Standlee & Associates, Inc. utilizing established acoustical sound propagation equations presented in reference materials such as "Handbook of Acoustical Measurements and Noise Control, Third Edition" by Cyril M. Harris (Mcgraw-Hill Inc., 1991). The model developed to calculate the future mining noise levels reaching a receiver includes the reduction of sound (sound attenuation) due to distance, atmospheric conditions, trees and terrain.

Reference sound level data for the various pieces of equipment was obtained from measurements made at the existing crushing and screening operation and from manufacturers of equipment owned by J.L. Storedahl & Sons, Inc.

The octave band sound pressure levels used in predicting the noise radiating from each of the major noise sources expected at the proposed site are presented in Table 3.

Table 3
Reference Sound Data Used in Predicting Mining Related Noise Levels¹

Source	Ref.	Octave Band Center Frequency (hz) Sound Pressure Levels (dB)							
	Dist. (ft)	63	125	250	500	1000	2000	4000	8000
Komatsu WA 500 FEL	50	71	76	68	70	69	66	61	53
Komatsu 650 Excavator	50	72	77	69	71	70	67	62	54
On-Site Haul Truck	50	72	81	83	77	73	67	60	50
Crushing & Screening Plant	50	82	87	85	86	85	84	83	83

Note 1: These levels were used to predict the hourly L_{25} noise level. The hourly L_{08} noise levels were predicted by adding 1 dB to the L_{25} noise levels. The hourly L_{03} noise levels were predicted by adding 3 dB to the L_{25} noise levels.

A computer version of the Federal Highway Administration, Noise Prediction Model was used to predict noise levels due to truck traffic associated with the project. The average and maximum number of daily truck trips were evaluated. This model calculates the sound pressure level at a receiver due to traffic flowing by the receiver at a constant speed. The model accounts for attenuations due to distance, barriers and vegetation.

9.3 Assumptions Included in the Analysis

To predict the worst case conditions that might exist with the mining extension, it was assumed that all the excavation and crushing equipment is operating continuously throughout each hour of the work day. All trucks are assumed to be traveling at 20 mph on site and 35 mph on county roads.

The sound levels at the residences in the valley will be influenced by the vegetation on the mining area. During the growing season, fields of hay or grain is grown on the land in the mining area. During the winter months, the ground is either plowed or a winter crop is planted. The influence of vegetation on the sound reaching the residences in the valley are considered valid only until the excavation removes the vegetation and the fields are replaced by water.

The sound radiating to the residences on the rim of the valley will not be affected by the vegetation in the valley and there will be only a minimal amount of effect by the vegetation on the valley walls. During the initial visits to the area in August 1991, the vegetation on the north slopes of the valley was noted to be mainly conifer trees while the vegetation on the south slope appeared to be mainly deciduous trees.

9.4 Prediction Results

Table 4 presents the predicted maximum Daybreak mine generated hourly L_{25} sound levels with no mitigation measures at the 17 prediction locations considered in this study.

 $Table\ 4$ Predicted Loudest Hour L₂₅ Sound Levels from Excavation & Crushing Operations at the Daybreak Mine Site with Approved Expansion of the Mining Area (levels in excess of the WAC limit are in bold)

Receiver	Crusher Noise (dBA)	Excavation Noise (dBA) (by phase)							Crushing plus Excavation Noise (dBA) (by phase)						
		1	2	3	4	5	6	7	1	2	3	4	5	6	7
1	44	49	67	46	40	42	34	34	50	67	48	45	46	44	34
2	48	70	62	51	46	49	40	42	70	62	52	50	52	49	48
3	46	47	55	55	43	43	37	37	50	56	56	48	48	47	47
4	46	47	51	58	44	44	38	38	50	52	58	48	48	47	47
5	46	46	49	63	45	45	39	39	49	51	63	42	49	47	47
6	46	47	51	70	51	51	42	42	50	52	70	52	52	47	47
7	46	48	51	70	52	52	43	43	50	52	70	53	53	48	48
8	46	48	51	63	67	56	44	44	50	52	63	67	56	47	47
9	46	48	51	62	65	55	44	44	50	52	62	65	56	48	48
10	46	46	50	55	62	53	45	45	49	51	56	62	54	49	49
11	46	45	44	46	61	50	52	52	49	48	49	61	51	53	53
12	46	40	38	38	45	43	55	48	47	47	47	49	48	56	50
13	48	40	38	38	45	43	55	48	49	48	48	50	49	56	51
14	48	40	38	38	45	43	55	48	49	48	48	50	49	48	48
15	48	41	46	54	43	43	37	37	49	50	55	49	49	48	48
16	46	43	42	42	38	40	38	38	48	47	47	47	47	47	47
17	50	39	39	39	38	39	39	40	50	50	50	50	50	50	50

10.0 IMPACT ASSESSMENT

The residences most likely to be impacted by the expansion of the mining area at the Daybreak mining site will be those residences located on the north rim of the valley overlooking the mining site, those residences located at the valley floor near the north and east boundaries of the expansion area and those residences located along Bennett Rd in the vicinity of the expansion area. The noise at residences south of the Lewis River (such as prediction locations 16 and 17 in Figure 2) will basically experience the same sound levels that were experienced prior to the mining expansion because they are so far from the proposed excavation area. Based on assessment using all three criteria, the noise reaching the residences south of the river will be "insignificant". Therefore, no noise mitigation measures are

required to reduce the noise radiating from the expansion area to residences on the south side of the Lewis River.

At prediction location 1 (Foster Residence), the loudest hour L_{25} noise level is expected to exceed the WAC noise criteria (60 dBA), the County SEPA criteria (55 dBA for this location) and the 10 dB increase criteria (60 dBA for this location) during excavation operations in Phase 2A if mitigation measures are not used to reduce the noise radiating from the excavation equipment. Therefore, noise impacts are expected to be "serious" at location 1 during mining activities in Phase 2A if noise mitigation measures are not included in the mining plan. During all other phases, the noise reaching the residence is expected to be below the noise levels already found at the residence so the noise impacts are expected to be "insignificant" during those phases. No noise mitigation will be required during those phases.

At prediction location 2 (Rose Residence), the loudest hour L_{25} noise level is expected to exceed the WAC noise criteria (60 dBA), the County SEPA criteria (60 dBA for this location) and the 10 dBA change criteria (65 dBA for this location) during some excavation operations in Phase 1A, 1C. 2B and 2C if mitigation measures are not used to reduce the noise radiating from the excavation equipment. Therefore, noise impacts would be considered "serious" at location 2 during mining activities in those phases if noise mitigation measures are not included in the mining plan. During all other phases, the noise reaching the residence is expected to be below that already found at the residence and therefore, noise impacts are expected to be "insignificant" during those phases. Consequently, no noise mitigation will be required during those phases.

At prediction location 3 (Morris Residence), the loudest hour L_{25} noise level is expected to remain below the WAC criteria limit and the 10 dB change limit at all times. However, the loudest hour L25 noise level is expected to exceed the County SEPA criteria (53 dBA for this location) at some time during excavation operations in Phase 2C and Phase 3 if mitigation measures are not used to reduce the noise radiating from the excavation equipment. Therefore, using the County SEPA criteria, the noise impact at location 3 could be considered "significant" during some portion of the excavation activities in Phase 2C and Phase 3. However, because the change will be less than 10 dB, the change in noise level is not considered "serious" during Phase 2C and Phase 3 activities. The noise reaching location 3 would be considered "insignificant" during activities in all other phases in the expansion area and noise mitigation measures will not be needed to protect prediction location 3 during those phases. Noise mitigation may be desirable during mining operations in portions of Phase 2C and 3.

At prediction locations 4 (Snider Residence) and 5 (Antes Residence), if mitigation measures are not used ,the loudest hour L₂₅ noise level is expected to exceed the County SEPA criteria level (53 dBA for location 4 and 52 dBA for location 5) but not the WAC criteria nor the 10 dBA change criteria (58 dBA for location 4 and 57 dBA for location 5) during some of the excavation operations in Phase 3. Therefore, noise impacts at locations 4 and 5 are expected to be "significant" during portions of the mining activities in Phase 3 but not "serious" because the levels will not exceed the WAC criteria nor the 10 dB change criteria mining activities in all other phases. During mining activities in all other phases, the noise reaching the two residences will remain below all three criteria and the noise impacts would be considered "insignificant" during those phases. Mitigation measures may be desirable during some parts of the Phase 3 mining, but during mining operations in all other phases, noise mitigation measures are not needed.

At prediction locations 6 (Gelfand Residence) and 7(Dorcheus Residence), the loudest hour L_{25} noise

level is expected to exceed the WAC noise criteria (60 dBA), the County SEPA criteria (52 dBA for location 6 and 53 dBA for location 7) and the 10 dBA change criteria (57 dBA for location 6 and 58 dBA for location 7) at some time during excavation operations in the Phase 3 area if mitigation measures are not used to reduce the noise radiating from the excavation equipment. Therefore, the noise during that time would be expected to have a "serious" impact on the two residences if mitigation was not considered. During all other phases, the noise reaching the two residences will always be below all three criteria and the impacts would be considered "insignificant" at the residences. Therefore, mitigation measures are needed only during mining activities in Phase 3 to protect locations 6 and 7.

At prediction locations 8 (2^{nd} Dorcheus Residence) and 9 (3^{rd} Dorcheus Residence), the loudest hour L_{25} noise level is expected to exceed the WAC noise criteria (60 dBA), the County SEPA criteria (54 dBA for location 8 and 53 dBA for location 9) and the 10 dBA change criteria (59 dBA for location 8 and 58 dBA for location 9) at some time during excavation operations in both the Phase 3 area and the Phase 4 area if mitigation measures are not used to reduce the noise radiating from the excavation equipment. Therefore, the noise during some part of Phase 3 and Phase 4 work would be expected to have a "serious" impact on the two residences if mitigation is not considered and mitigation of the noise during those phases is very important. During Phase 5 the noise levels at the two residences will be slightly above the County SEPA criteria levels so that the impact might be considered "significant" but the levels would not be high enough to raise the impact assessment to "serious". Noise mitigation may be desirable during mining operations in portions of Phase 5. During phases 1, 2, 6 and 7, the noise reaching the two residences will be below all three criteria and the impacts would be considered "insignificant" and mitigation measures are not needed during those phases.

The noise radiating from the Daybreak site to location 10 (Crawford Residence) would not exceed the three criteria during mining activities in Phase 1, 2, 5, 6 and 7 and thus the impacts during those phases would be considered "insignificant" and mitigation measures are not needed during that time. During mining activities in Phase 4, the noise reaching location 10 would, at times, exceed the WAC criteria (60 dBA), the County SEPA criteria (54 dBA for this location) and the 10 dB change criteria (59 dBA for this location). At that time, the noise radiating from the mining operations to the location would be considered "serious" and mitigation would be highly desirable. During mining activities in Phase 3, the noise radiating to location 10 would be only slightly above the County SEPA criteria without mitigation but it would not exceed the other two criteria. Therefore the noise reaching location 10 during Phase 3 would not be considered "serious" but noise mitigation may be desirable during mining operations in portions of Phase 3.

At location 11 (Hanger Residence), the noise radiating from the mining site would be considered "insignificant" during all phases except Phase 4 when the noise reaching the location could possible exceed all three criteria (the WAC code limit of 60 dBA, the SEPA criteria of 54 dBA and the 10 dB change limit of 59 dBA), if noise mitigation measures are not considered during that phase. Therefore, mitigation measures should be provided for location 11 during Phase 4 mining activities. During all other phases, mitigation of noise would not be necessary.

At location 12 (Woodside Residence), the noise radiating from the mining activities in the expansion area will be "insignificant" during all phases except Phase 6 because during the mining in those phases, the noise will always be less than all three criteria levels (60 dBA for the WAC limit, 52 dBA for the County SEPA criteria and 57 dBA for the 10 dB increase criteria). Thus during mining activities in Phase 1, 2, 3, 4, 5 and 7, mitigation of noise from the mining area is not necessary. During the mining

in the Phase 6 area, there is the potential that at some time, the noise radiating to location 12 may be more than 5 dB above the ambient but it will not be more than 8 dB above the ambient which means it will not be a "serious" change. Noise mitigation may be desirable during mining operations in portions of Phase 6.

At locations 13 (Sass Residence), 14 (Anderson Residence), 15 (Bleth Residence), 16 (unknown residence owner), and 17 (unknown residence owner) the noise radiating from the expansion site will always be below all three criteria. Therefore, there will be an "insignificant" change in noise at those sites due to the expansion and mitigation is not needed.

11.0 MITIGATION MEASURES

According to the impact assessment results, mitigation measures "will be required" to reduce the amount of excavation noise that will radiate from mining activities in Phase 1 to residences in the vicinity of location 2, from mining activities in Phase 2 to residences in the vicinity of location 1 and 2, from mining activities in Phase 3 to residences in the vicinity of prediction locations 6, 7, 8, and 9, and from mining activities in Phase 4 to residences in the vicinity of location 8, 9, 10 and 11. Also, according to the results, it may be "desirable" to consider providing mitigation measures during mining activities in Phase 2 for residences in the vicinity of location 3 and location 6, during mining activities in Phase 3 for residences in the vicinity of location 3, 4, 5 and 10, during mining activities in Phase 5 for residences 8 and 9 and during mining activities in Phase 6 for location 12.

To reduce the noise levels radiating from the mining area to levels that would be considered to have an "insignificant" impact on residences, berms or engineered barriers could be constructed at specific locations around the mining area. Figure 3 presents the locations for berms or engineered barriers and Table 5 shows the height and length required for the berms or barriers.

TABLE 5
Required Barrier Heights and Lengths
to Achieve "Insignificant" Noise Impacts at All Residences

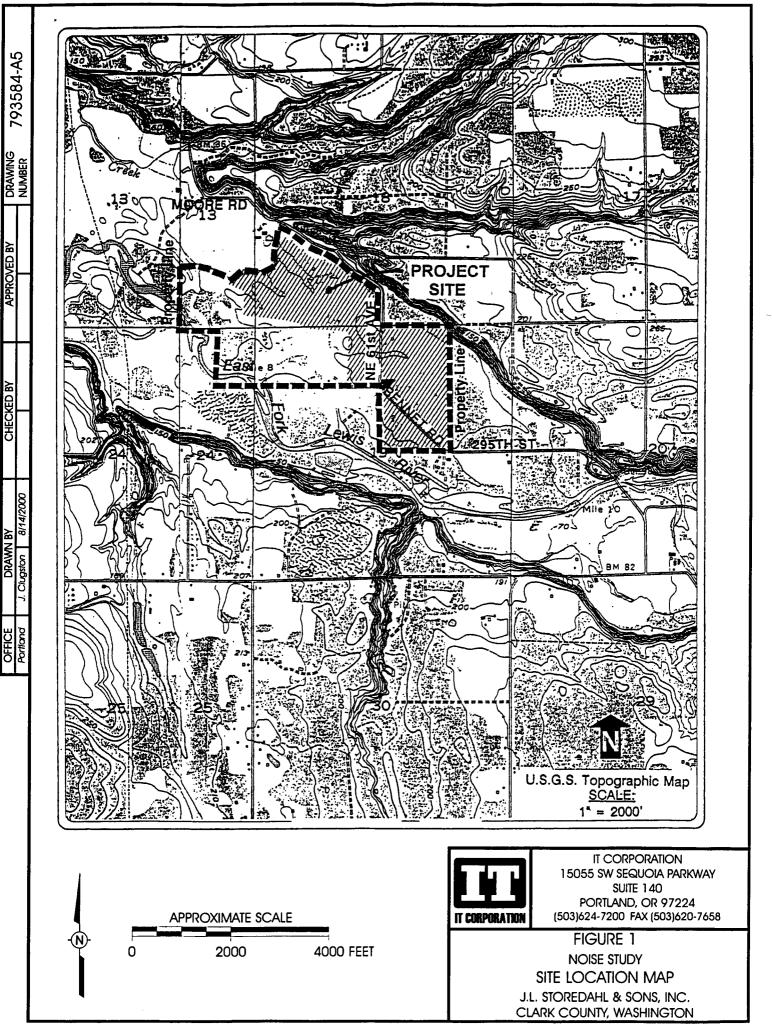
Dimensions		Barrier#										
		1	2	3	4	5	6	7	8	9	10	
Length (feet)		300	200	400	200	300	850	700	600	550	400	
H E I G H T (ft)	left end (as seen from residences)	8	9	9	9	9	1	10	9	1	5	
	100' from left end	11	9.5	9	8	9	2	11	9	2	5	
	200' from left end	11	9	5	8	9	4	12	7	4	5	
	300' from left end	11	NA	2	NA	9	4	10	3	7	4	
	400' from left end	NA	NA	2	NA	NA	8	9	6	6	2	
	500' from left end	NA	NA	NA	NA	NA	8	8	6	5	NA	
	600' from left end	NA	NA	NA	NA	NA	8	8	5	NA	NA	
	700' from left end	NA	NA	NA	NA	NA	8	9	NA	NA	NA	
	800' from left end	NA	NA	NA	NA	NA	8	NA	NA	NA	NA	

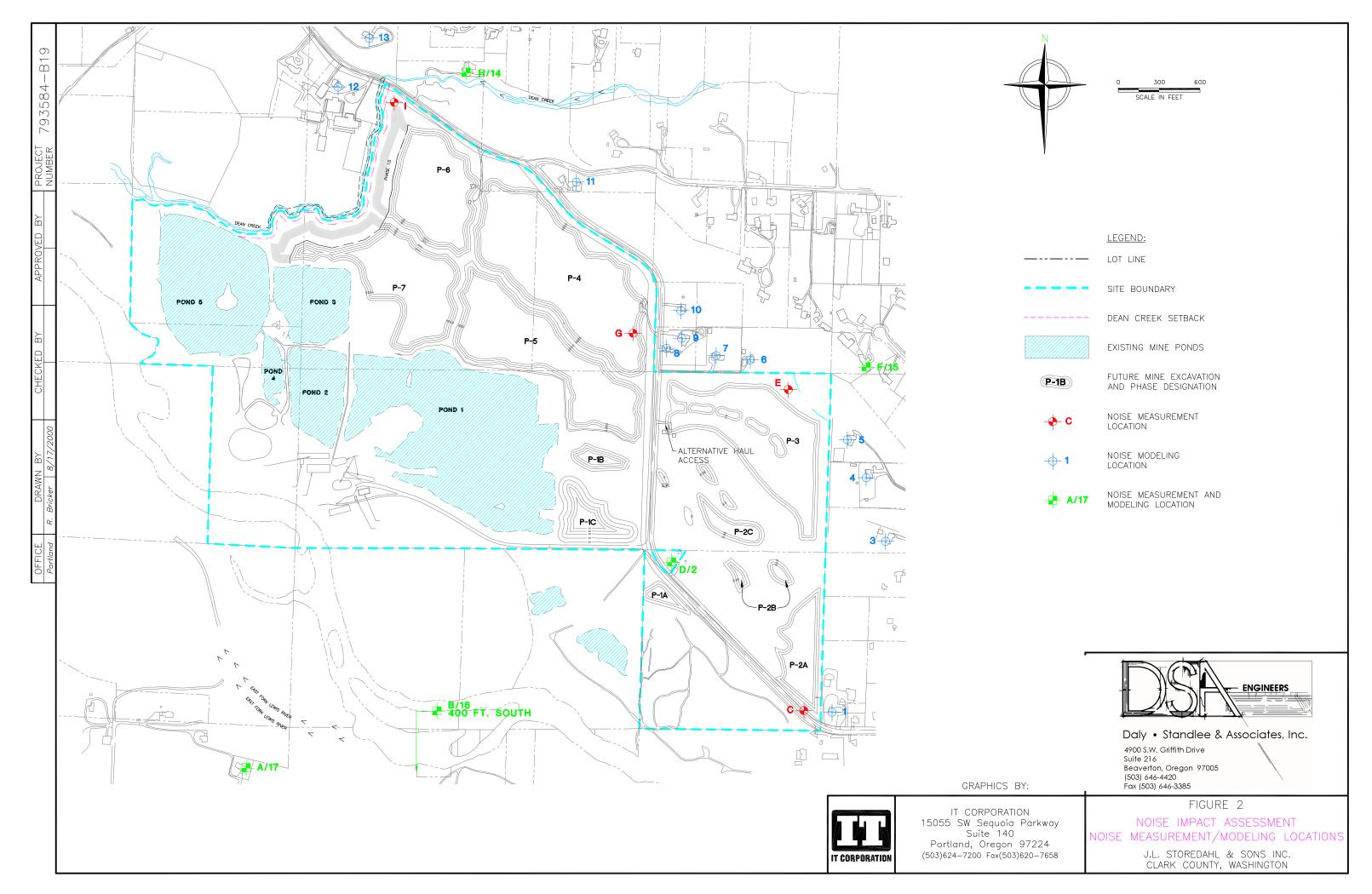
Barrier # 1 is required prior to excavation in Phase 1A. Once excavation is complete in Phase 1A, the barrier is no longer required. Barrier #2 is required prior to excavation in Phase 1C. After excavation is complete in Phase 1C, the barrier is no longer required. Barrier #3 and Barrier #6 is required after the conveyor feed hopper has been installed in the Phase 3 area and prior to excavation in Phase 2A. Once excavation is complete in Phase 2A, Barrier #3 is no longer required but Barrier #6 needs to remain until excavation is complete in the east half of Phase 3. Barrier #4 is required prior to excavation in Phase 2B. Once excavation is complete in Phase 2B, the barrier is no longer required. Barrier #5 is required prior to excavation in Phase #2C. Once excavation is complete in Phase 2C, the barrier is no longer required. Barrier #7 is required prior to excavation in the western portion of Phase 3. Barrier #7 should remain until excavation is complete in the Phase 3 area. Barrier #8 is required prior to excavation in Phase 4. Barrier #8 should be left until excavation is complete in the western end of Phase 4 and Phase 5. Barrier #9 is required prior to excavation in the northern portion of Phase 4. Once the northern portion of Phase 4 has been excavated, the barrier can be removed. Barrier #10 needs to be constructed prior to excavation in Phase 1D. The barrier should be left until excavation is complete in the western half of Phase 6.

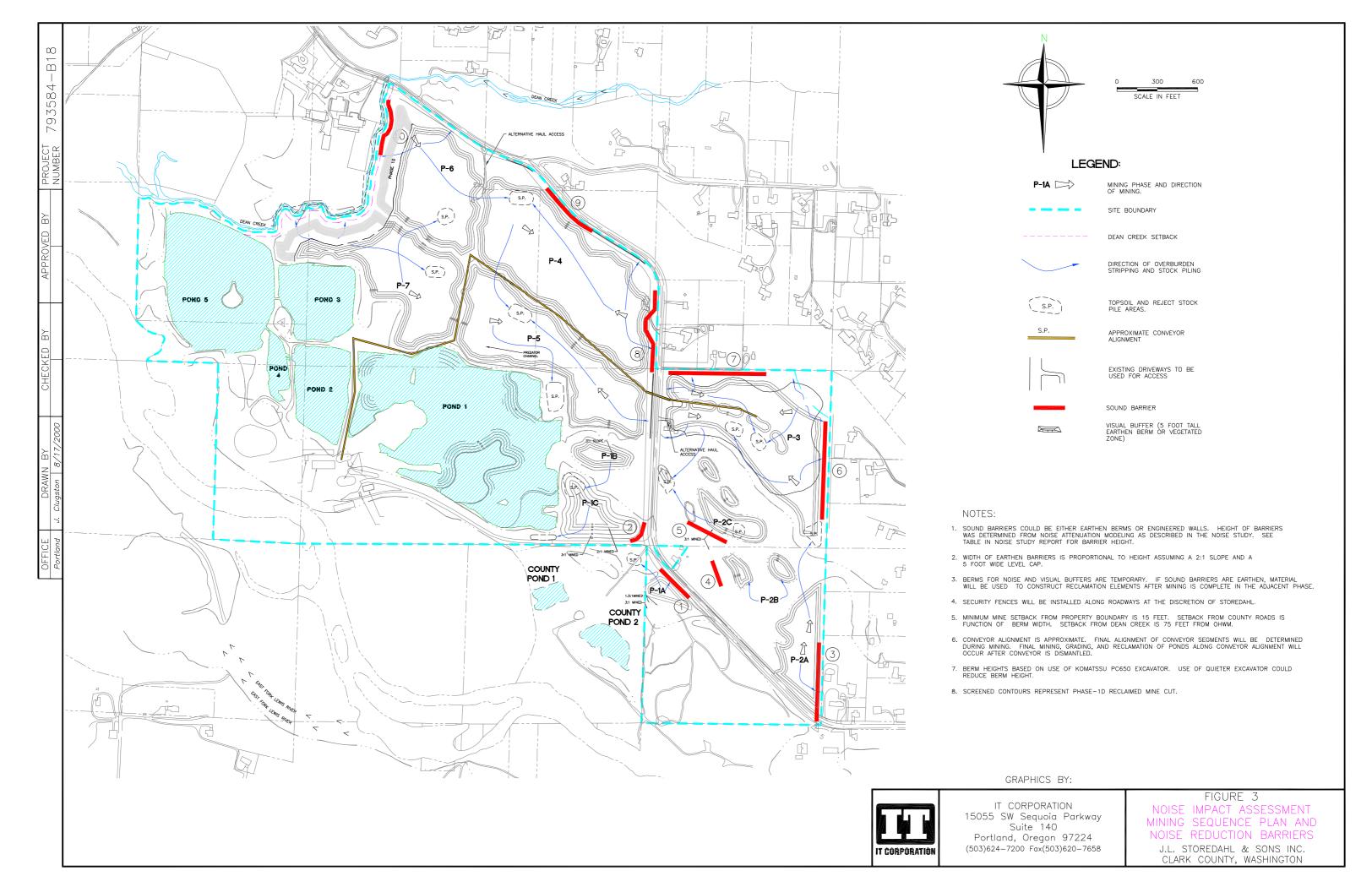
12.0 CONCLUSIONS

Mining can occur in the proposed expansion area at Daybreak Gravel Mine with "insignificant" noise impacts on residences around the area if berms or engineered barriers are placed at specific locations shown in Figure 3 with the length and heights shown in Table 5. Barrier # 1 is required prior to excavation in Phase 1A. Once excavation is complete in Phase 1A, the barrier is no longer required. Barrier #2 is required prior to excavation in Phase 1C. After excavation is complete in Phase 1C, the barrier is no longer required. Barrier #3 and Barrier #6 is required after the conveyor feed hopper has 159916-1.rep

been installed in the Phase 3 area and prior to excavation in Phase 2A. Once excavation is complete in Phase 2A, Barrier #3 is no longer required but Barrier #6 needs to remain until excavation is complete in the east half of Phase 3. Barrier #4 is required prior to excavation in Phase 2B. Once excavation is complete in Phase 2B, the barrier is no longer required. Barrier #5 is required prior to excavation in Phase #2C. Once excavation is complete in Phase 2C, the barrier is no longer required. Barrier #7 is required prior to excavation in the western portion of Phase 3. Barrier #7 should remain until excavation is complete in the Phase 3 area. Barrier #8 is required prior to excavation in Phase 4. Barrier #8 should be left until excavation is complete in the western end of Phase 4 and Phase 5. Barrier #9 is required prior to excavation in the northern portion of Phase 4. Once the northern portion of Phase 4 has been excavated, the barrier can be removed. Barrier #10 needs to be constructed prior to excavation in Phase 1D. The barrier should be left until excavation is complete in the western half of Phase 6.







APPENDIX

WAC 173-60-040 Maximum permissible environmental noise levels. ¹ (1) No person shall cause or permit noise to intrude into the property of another person which noise exceeds the maximum permissible noise levels set forth in this section.

(2)(a) The noise limitations established are as set forth in the following table after any applicable adjustments provided for herein are applied.

EDNA of NOISE SOURC		EDNA o RECEI	f VING PROPERTY
C	class A C	lass B	Class C
CLASS A	55 dB	A 57 dB	A 60 dBA
CLASS B	57	60	65
CLASS C	60	65	70

(b) Between the hours of 10:00 p.m. and 7:00 a.m. the noise limitations of the foregoing table shall be reduced by 10 dBA for receiving property within Class A EDNA's.

⁽c) At any hour of the day or night the applicable noise limitations in (a) and (b) above may be exceeded for any receiving property by no more than:

⁽i) 5 dBA for a total of 15 minutes in any one-hour period; or

⁽ii) 10 dBA for a total of 5 minutes in any one-hour period; or

⁽iii) 15 dBA for a total of 1.5 minutes in any one-hour period. [Order 74-32, Section 173-60-040, filed 4/22/75, effective 9/1/75]

Washington State Noise Code, Chapter 173-60 WAC, Maximum Environmental Noise Levels,
 March 4, 1987
 159916-1.rep
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Measured Octave Band Sound Levels Of the Excavation and Crushing Operations Equipment

Source	Referenc Dist (ft)	o	31.5	63	125	Octav 250	e Band 500	Octave Band Center Frequency (hz 250 500 1000 2000 4000	Frequen 2000	cy (hz) 4000	8000	16000
Excavation Equipment: Terex 90C Wheel Loader Komatsu Backhoe	44 100		61 61	69 72	79 77	72 69	67 71	70 70	67 79	59 62	52 54	42 39
Crushing Equipment: Roll Crusher	17		98	85	92	68	68	68	68	68	06	94
Jaw Crusher	10		98	92	94	93	93	91	88	83	79	99
Cone Crusher 9	œ	_	88	94	94	96	94	91	85	77	64	
Primary Screen Deck 20	82	2	81	98	83	83	81	84	84	84	73	
1" minus Screen Deck	25		62	79	98	83	84	81	83	82	80	72
1/4" minus Screen Deck	15		77	80	84	83	83	79	78	9/	74	62
Terex 90B Wheel Loader	12		73	70	85	83	84	82	83	9/	72	65
Terex 3305B Haul Truck	38		72	74	83	85	79	75	73	69	62	52

Date:	7/27/00					Projec	et Num	ber: 1	59916			
Project Name:	Daybreak Mining S	ite - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction to determ with no reduction of of pit 1A- Saved in	f FEL n	oise an	d assur	ming ex	cavato				eiver 4	(Rose]	Residenc
Number of source Number or receiv Maximum reduct		ier: 24				Temp Humi	erature dity:	: 50□ 70□				
					Refer	ence Le	evels					
Source	Ref Dis	t dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 500 Terex 90 Wheel I		73.3□ 73.9□	79.1 \(\text{80.9} \)		 76□ 79□	 68□ 72□	70□ 67□	 69□ 70□	66□ 67□	61 □ 59 □	53 □ 52 □	
	Receiver 4 - Rose R with barrier(s): without barrier(s): provided by barrier(s)	61.5□ 70.3□	dBA dBA	76.	2□dB 6□dB ·□ dB							
					Level	with a	nd with	out bar	rier			
Source		dBA	dB	63	125	250	500	1k	2k_	4k	8k	
Komatsu WA 500	FEL w/ barrier	60.9□	69.3□	62□	67□	58□	59□	56□	51□	$42\square$	$31\square$	
Terex 90 Wheel I	w/out barrier Loaderw/ barrier w/out barrier	52.6□	75.5 □ 63.2 □ 69.9 □	52□	72 □ 62 □ 68 □	64□ 54□ 61□	66□ 47□ 56□	65□ 48□ 59□	62 □ 42 □ 56 □	56□ 30□ 46□	48□ 20□ 39□	
Receiver		X	Y		Z							
Receiver 4 - Rose	e Residence	$0\Box$	0]	5□							
		Sc	ource C	oordin	ates		Barrie	er Coor	dinates		Γrees	
Source Name		X	Y		Z	X		Y	Z		ft	
Komatsu WA 500) FEL		$\overline{0}$]	<u>10</u> \Box	14	0 🗆	$\overline{0}$	12		$\overline{0}$	
Terex 90 Wheel I	Loader	155□	0]	$10\Box$	14	$0 \square$	$0\square$	13		$0\square$	

Date:	7/27/00					Projec	et Num	ber: 1	59916			
Project Name:	Daybreak Mining S	ite - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction to determ with no reduction of of pit 1A- Saved in	f FEL n	oise an	d assuı	ming ex	cavato					(Rose I	Residenc
Number of source Number or receiv Maximum reduct		ier: 24[Temp Humi	erature dity:	: 50□ 70□				
					Refer	ence Le	evels					
Source	Ref Dis	t dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 500 Terex 90 Wheel I		73.3□ 73.9□	79.1 \(\text{80.9} \)		 76□ 79□	 68□ 72□	70□ 67□	 69□ 70□	 66□ 67□	61 □ 59 □	53 □ 52 □	
	Receiver 4 - Rose R with barrier(s): without barrier(s): provided by barrier(s)	60.8□ 67.8□	dBA dBA	74.	.5□dB .1□dB '□ dB							
					Level	with a	nd with	out bar	rier			
Source		dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 500	FEL w/ barrier		67.5□		65□	56□	58□	56□	51 🗆	43 🗆	32 🗆	
	w/out barrier		73.0		70□	62□	64□	63□	59□	53□	45 □	
Terex 90 Wheel I	_oaderw/ barrier w/out barrier		61.6□ 67.7□		60□ 66□	53 □ 59 □	47□ 54□	48□ 57□	42 □ 53 □	30□ 44□	20□ 37□	
Receiver		X	<u>Y</u>		<u>Z</u>							
Receiver 4 - Rose	e Residence	$0\square$	0		$5\square$							
		So	ource C	oordin	ates		Barrio	er Coor	dinates]	Γrees	
Source Name		X	Y		Z	X		Y	Z		ft	
Komatsu WA 500) FEL	200 □	$\overline{0}$		<u>10</u>	18	$0 \square$	$\overline{0}$	11		$\overline{0}$	
Terex 90 Wheel I	Loader	200□	0		10□	18	$0 \square$	$0\Box$	12	, 🗌	$0\Box$	

Date:	7/27/00						Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak 1	Mining Si	te - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction with no recof pit 2A-	duction of	FEL n	oise an	d assuı	ning th	e FEL		-				Reside
Number of source Number or receive Maximum reduct	vers: 1□	d by barri	er: 24[Temp Humi	erature dity:	e: 50□ 70□				
						Refer	ence L	evels					
Source		Ref Dist	dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL	100 🗆	73.3 □	7 9.1□	71 🗆	76 □	68 □	70 □	69 □	66 🗆	61 🗆	53□	
Receiver 1: Total noise level Total noise level Noise reduction	without bar	(s): rier(s):	55.3 ☐ 72.3 ☐	dBA dBA	78.	2□dB 2□dB 0□dB							
						Level	with a	nd with	out ba	rrier			
Source			dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50		rrier t barrier				65□ 75□	54□ 67□	53 □ 69 □		43 □ 65 □	35□ 59□	27□ 51□	
Receiver			X	Y		Z							
Residence 3 - We	olle Residen	ce	$\overline{0}$	$\overline{0}$]	$\frac{Z}{5\Box}$							
			Se	ource C	oordin	ates		Barrio	er Coor	dinates]	rees	
Source Name			X	Y		<u>Z</u>	X		Y	Z		ft	
Komatsu WA 50	0 FEL		<u>110</u> □	$\overline{0}$]	<u>-2</u> □	90)	$\overline{0}$	8		$\overline{0}$	

Date:	7/27/00				Proje	ct Num	ber: 1	59916			
Project Name:	Daybreak Minin	g Site - Am	ended Mini	ng Plan	NEngin	neer:y	K	GS			
Comments:	Prediction to det with no reductio of pit 2A- Saved	n of FEL no	ise and assu	ıming F	EL is a					3 (Woll	e Reside
Number of source Number or receive Maximum reduced		oarrier: 24□			Temp Humi	erature dity:	2: 50□ 70□				
				Refer	ence L	evels					
Source	Ref	Dist dBA	dB 63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL 10	73.3□	79.1 🗆 71 🗆	76 □	68 □	70 □	69 🗆	66 🗆	61 🗆	53 🗆	
	Residence 3 - W with barrier(s): without barrier(s) provided by barrier	55.8□d 57.5□d	IBA 62 IBA 64	2.7□dB 4.6□dB 8□ dB							
				Level	with a	nd with	out bar	rrier			
Source		dBA	dB 63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL w/out barri	$\overline{54.8}$	61.5 🗆 54 🗆	59 □	51 🗆	52 □	51 🗆	47 🗆	36□	<u></u>	
Receiver		X	Y	$\frac{Z}{5}$							
Residence 3 - We	olle Residence	$0\square$	$0\square$	5□							
		Soi	urce Coordi	nates		Barrie	er Coor	dinates	;]	Trees	
Source Name		X	Y	Z	X	_	Y	Z		ft	
Komatsu WA 50	0 FEL	730□	$\overline{0}$	<u>10</u>	0		$\overline{0}$	0		$\overline{0}$	

Date:	7/27/00						Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak N	Mining Si	te - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction with no red of pit 2A-S	luction of	FEL n	oise an	d assu	ning th	e FEL		-			•	Reside
Number of sourc Number or receiv Maximum reduct	vers: 1□	l by barri	er: 24[Temp Humi	erature dity:	e: 50□ 70□				
	r	,				Dafar	ence Le	avalc					
Source		Ref Dist	dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL	100 🗆	73 .3 □	7 9.1□	71 🗆	76 □		$\overline{70}$		66 □	6 1□	53 □	
Receiver 1: Total noise level Total noise level Noise reduction p	without barr	(s): rier(s):	53.4□ 58.5□	dBA dBA	64.	.9□dB .9□dB 0□ dB							
						Level	with a	nd with	out bar	rrier			
Source			dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50		rrier barrier		59.9□ 64.9□		57□ 62□	49□ 54□	51□ 56□	49 □ 54 □	45 □ 51 □	37□ 42□	28□ 33□	
Receiver			X	Y		Z							
Residence 3 - Wo	olle Residen	ce	$\overline{0}$	$\overline{0}$]	$\frac{Z}{5\Box}$							
			So	ource C	oordin	ates		Barrie	er Coor	dinates]	rees	
Source Name			X	Y		Z	X		Y	Z		ft	
Komatsu WA 50	0 FEL		<u>500</u> □	$\overline{0}$]	<u>-2</u> □	$\frac{-}{27}$	75□	$\overline{0}$	$\overline{2}$		$\overline{0}$	

Date:	7/27/00					Projec	et Num	ber: 1	59916			
Project Name:	Daybreak Mining S	ite - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction to determ with no reduction o of pit 2A- Saved in	f FEL n	oise an	d assu	ming th	e FEL						de
Number of source Number or receiv Maximum reduct		ier: 24[Temp Humi	erature dity:	50□ 70□				
					Refer	ence Le	evels					
Source	Ref Dis	t dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL 100□	73.3	79 .1□	71 🗆	76 □	68 □	70 □	69 □	66	61 🗆	53□	
	Residence 3 - Wollowith barrier(s): without barrier(s): provided by barrier(s)	54.8□ 63.9□	dBA dBA	70.	.6□dB .0□dB ŀ□ dB							
Source		dBA	dB	63	Level 125	with an 250	nd with 500	out baı 1k	rier 2k	4k	8k	
Komatsu WA 50	0 FEL w/ barrier w/out barrier	 54.8□	63.6 \(\text{70.0} \)		$\frac{123}{61} \square$ $67 \square$	52□ 59□	53□ 61□	50□ 60□	2K 44□ 56□	35□ 49□	23 \(\tau \)	
Receiver		X	Y		Z							
Residence 3 - Wo	olle Residence	$\overline{0}$	$\overline{0}$		<u>5</u>							
		So	ource C	oordin	ates		Barrie	er Coor	dinates]	Trees	
Source Name		X	Y		<u>Z</u>	X		Y	\underline{Z}		ft	
Komatsu WA 50	0 FEL		$\overline{0}$		<u>-2</u> □	14	-0□	$\overline{0}$	7		$\overline{0}$	

Date:	7/27/00						Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak N	Mining Si	te - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction with no red of pit 3- Sa	luction of	FEL n	oise an	d assu	ming th			-			3 (Snider Re	sid
Number of source Number or receive Maximum reduct	vers: 1□	l by barri	er: 24[Temp Humi	erature dity:	2: 50□ 70□				
						Refer	ence Le	evels					
Source		Ref Dist	dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL	100 🗆	73 .3□	79 .1□	7 1□	76 □	68 □	70 □	69 □	66 □	6 1□	53□	
Receiver 1: Total noise level Total noise level Noise reduction p	without barr	(s): rier(s):	52.6□ 57.6□	dBA dBA	64.	.1□dB .1□dB 0□ dB							
							with a		out bai				
Source			dBA	dB —	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50		rrier barrier		59.1 □ 64.1 □		56□ 61□	48□ 53□	50□ 55□	49□ 54□	45□ 50□	36□ 41□	27 □ 32 □	
Receiver			X	Y		<u>Z</u>							
Residence 5B - S	nider Reside	ence	$\overline{0}$	$\overline{0}$]	<u>5</u>							
			So	ource C	oordin	ates		Barrie	er Coor	dinates]	rees	
Source Name			X	Y		Z	X		Y	Z		ft	
Komatsu WA 50	0 FEL			$\overline{0}$]	<u>10</u> □	30	00 🗆	$\overline{0}$	8		$\overline{0}$	

Date:	7/27/00					Projec	ct Num	ber: 1:	59916		
Project Name:	Daybreak Mining S	ite - An	nended	Mining	g Plan 1	NEngin	eer:y	K	GS		
Comments:	Prediction to determ with no reduction of of pit 3- Saved in fit	f FEL n	oise and	d assur	ning th			-			(Antes
Number of source Number or receive Maximum reduct		ier: 24[Temp Humi	erature dity:	: 50□ 70□			
					Refere	ence Le	evels				
Source	Ref Dis	t dBA	dB	63	125	250	500	1k	2k	4k	8k
Komatsu WA 50	0 FEL 100□	73 .3□	79 .1□	7 1□	76 □	68 □	70 □	69 □	66 □	61 □	53 □
	Residence 5 - Antes with barrier(s): without barrier(s): provided by barrier(s)	54.3 ☐ 59.5 ☐	dBA dBA	65.	8□dB 9□dB □ dB						
Source Komatsu WA 50	0 FEL w/ barrier w/out barrier		dB 60.8□ 65.9□		Level 125 58□ 63□	with an $\frac{250}{50}$	nd with $\frac{500}{52}$	fout bar $\frac{1k}{50}$	rrier 2k 46□ 52□	4k 38□ 43□	8k 29□ 35□
	w/out barrier	39.3□	03.9	<i>3</i> 6□	03 🗆	<i>33</i> 🗆	31	<i>33</i> \Box	<i>32</i> \Box	43	<i>33</i> 🗆
Receiver		X	Y		\underline{Z}						
Residence 5 - An	tes Residence	$0\Box$	$\overline{0}$		<u></u>						
		So	ource C	oordin	ates		Barrie	er Coor	dinates		Γrees
Source Name		X	<u>Y</u>		<u>Z</u>	X		<u>Y</u>	$\frac{Z}{Z}$		ft
Komatsu WA 50	0 FEL	450□	$0\Box$		$10\square$	18	\Box	$0\square$	8		$0\Box$

Residen

Date:	7/27/00						Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak N	Iining Si	te - An	nended	Minin	g Plan l	NEngin	eer:y	K	GS			
Comments:	Prediction t with no red of pit 3- Sa	uction of	FEL n	oise an	d assu	ming th							(esiden
Number of sourc Number or receiv Maximum reduct	vers: 1□	by barri	er: 24[Temp Humi	erature dity:	e: 50□ 70□				
	1	J				Refer	ence Le	evelc					
Source		Ref Dist	dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL	100 🗆	73 .3□	79 .1□	71 □	76 □		70 □	69 □	66 □	6 1□	53 □	
Receiver 1: Total noise level Total noise level Noise reduction p	without barr	s): ier(s):	52.2□ 63.2□	dBA dBA	69.	.2□dB .4□dB 5□ dB							
						Level	with a	nd with	out bar	rrier			
Source			dBA	dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50		rier barrier		62.2□ 69.4□		60□ 66□	51□ 58□	51 □ 60 □	47□ 59□	41 □ 56 □	31□ 48□	19□ 40□	
Receiver			X	Y		Z							
Residence 5B - S	nider Reside	nce	$\overline{0}$	$\overline{0}$		$\frac{Z}{5}$							
			So	ource C	Coordin	ates		Barrie	er Coor	dinates	٦	rees	
Source Name			X	Y		Z	X		Y	Z	-	ft	
Komatsu WA 50	0 FEL		 300□	$\overline{0}$		<u>-2</u> □	$\frac{1}{20}$	00 🗆	$\overline{0}$	8		$\overline{0}$	

Date:	7/27/00				Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak Minin	g Site - Am	ended Minii	ng Plan	NEngin	neer:y	K	GS			
Comments:	Prediction to det with no reductio of pit 3- Saved in	n of FEL no	oise and assu	iming th			-				r Resid
Number of source Number or receive Maximum reduced		oarrier: 24	l		Temp Humi	erature dity:	e: 50□ 70□				
				Refer	ence L	evels					
Source	Ref	Dist dBA	dB 63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL 10	73.3	79.1 🗆 71 🗆	76 □	68□	70 □	69□	66 🗆	61	53□	
	Residence 5B - S with barrier(s): without barrier(s) provided by barrie	52.2□¢ 58.9□¢	dBA 59	0.8□dB 5.3□dB 5□ dB							
Carrage		A CIL	JD (2		with a				41-	01-	
Source	0 PPI /1 :		$\frac{dB}{63} = \frac{63}{53}$	$\frac{125}{57}$	$\frac{250}{400}$	$\frac{500}{500}$	$\frac{1k}{40}$	$\frac{2k}{42}$	$\frac{4k}{22}$	$\frac{8k}{21}$	
Komatsu WA 50	0 FEL w/ barrier w/out barri		59.8□ 52□ 65.3□ 57□	57□ 62□	49□ 54□	50□ 56□	48□ 55□	43 □ 51 □	33 □ 43 □	21 □ 34 □	
	W/Out buill	30.7 L	03.3 🗆 37 🗆	02		<i>5</i> 0 🗆	<i>33</i> 🗆		15 🗆	<i>3</i> 1 🗆	
Receiver		X	Y	$\frac{\mathbf{Z}}{\mathbf{Z}}$							
Residence 5B - S	nider Residence	$\overline{0}$	$\overline{0}$	<u>5</u> □							
		So	urce Coordi	nates		Barrio	er Coor	dinates]	Trees	
Source Name		X	Y	$\frac{Z}{}$	X	_	Y	$\underline{\mathbf{Z}}$	_	ft	
Komatsu WA 50	0 FEL	$\overline{480}$	$\overline{0}$	<u>-2</u> □	32	20 🗆	$\overline{0}$	4		$\overline{0}$	

Date:	7/27/00				Project Number: 159916							
Project Name:	Daybreak Mining S	Site - Ame	ended Minii	ng Plan	NEngin	neer:y	K	GS				
Comments:	Prediction to determine with no reduction of pit 3- Saved in f	of FEL no	ise and assu	iming th			-			•	s Resid	
Number of source Number or receiv Maximum reduce		rier: 24□	Temperature: 50 ☐ Humidity: 70 ☐ er: 24 ☐									
				Reference Levels								
Source	Ref Di	st dBA	dB 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	0 FEL 100	73.3 🗆	79.1 🗆 71 🗆	76 □	68□	70 □	69□	66□	61 🗆	53□		
Total noise level	Receiver 1: Residence 5B - Snider Residence Total noise level with barrier(s): 51.7 dBA 58.8 dB Total noise level without barrier(s): 57.6 dBA 64.1 dB Noise reduction provided by barrier(s): 5.8 dBA 5.3 dB											
G.		ID A	1D (2		with a				41	01		
Source	0.777		$\frac{dB}{dB} = \frac{63}{51}$	$\frac{125}{760}$	$\frac{250}{100}$	$\frac{500}{100}$	$\frac{1k}{40}$	$\frac{2k}{12}$	$\frac{4k}{2a}$	$\frac{8k}{2}$		
Komatsu WA 50	0 FEL w/ barrier w/out barrier		58.8□ 51□ 64.1□ 56□	56□ 61□	48□ 53□	49□ 55□	48□ 54□	43 □ 50 □	33 □ 41 □	22□ 32□		
	w/out barrier	37.0□ (04.10 300	O1 \Box	<i>33</i> \Box	<i>33</i> \Box	JT	30 🗆	⊤ 1 □	<i>32</i> \Box		
Receiver		X	Y	\underline{Z}								
Residence 5B - S	Snider Residence	$\overline{0}$	$\overline{0}$	<u>5</u>								
		Sou	arce Coordi	nates		Barrie	er Coor	dinates]	Trees		
Source Name		X	Y	<u>Z</u>	X	_	Y	\mathbf{Z}	_	ft		
Komatsu WA 50	0 FEL	55 0□	$\overline{0}$	<u>-2</u> □	47	7 0□	$\overline{0}$	1		$\overline{0}$		

Date:	7/27/00				Projec	ct Num	ber: 1	59916				
Project Name:	Daybreak Mining S	ite - Ame	nded Minin	g Plan	NEngin	neer:y	K	GS				
Comments:	Prediction to determ to meet County 5 dl is 12' below grade i	B change	rule with no	reduct	tion of	FEL no	oise and	l assum	ing the	•	d Resido	
Number of source Number or received Maximum reduce		Temperature: 50 ☐ Humidity: 70 ☐ ier: 24 ☐										
Source	Ref Dis		B 63	125	ence Le 250	<u>500</u>	<u>1k</u>	2k	4k	<u>8k</u>		
Komatsu WA 50	00 FEL 100□	73.3□ 7	9.1□ 71□	76□	68□	70□	69□	66□	61□	53□		
Total noise level	Receiver 1: Residence 7 - Gelfand Residence Total noise level with barrier(s): 52.9 dBA 64.8 dB Total noise level without barrier(s): 69.5 dBA 75.5 dB Noise reduction provided by barrier(s): 16.6 dBA 10.7 dB											
Carmaa		ר א ערף	D 62		with a				41-	01-		
Source	. O. F. F		$\frac{B}{A} = \frac{63}{50}$	$\frac{125}{62}$	$\frac{250}{52}$	$\frac{500}{51}$	$\frac{1k}{4\pi}$	$\frac{2k}{11}$	$\frac{4k}{2a}$	$\frac{8k}{2}$		
Komatsu WA 50	00 FEL w/ barrier w/out barrier		4.8□ 59□ 5.5□ 67□	63 □ 72 □	52 □ 64 □	51□ 66□	47 □ 65 □	41 □ 62 □	32□ 56□	24 □ 48 □		
Receiver		X	Y	<u>Z</u>								
Residence 7 - Ge	elfand Residence	$0 \square$	$0\Box$	5□								
		Sou	rce Coordir	nates		Barrio	er Coor	dinates]	Γrees		
Source Name		X	Y	$\frac{\mathbf{Z}}{\mathbf{Z}}$	X	-	Y	\underline{Z}		ft		
Komatsu WA 50	0 FEL	150□	$0\Box$	- 2□	10	00 🗆	$0\square$	12	\Box	$0\square$		

Date:	7/27/00 Project Number: 159916										
Project Name:	Daybreak Mining	Site - Am	ended Mir	ning Plan	NEngin	eer:y	K	GS			
Comments:	Prediction to deter to meet 10 dB char is 12' below grade	nge rule w	vith no red	luction of	FEL no	oise and	d assun	ning the	FEL	(Gelfand	Resido
Number of sourc Number or receiv Maximum reduct		rier: 24□	Temperature: 50 ☐ Humidity: 70 ☐ r: 24 ☐								
				Refer	ence L	evels					
Source	Ref Di	st dBA	dB 63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL 100	73.3	79.1 🗆 71	76	68□	70 □	69□	66 🗆	61 🗆	53□	
Total noise level	Receiver 1: Residence 7 - Gelfand Residence Total noise level with barrier(s): 57.1 □ dBA 67.5 □ dB Total noise level without barrier(s): 69.5 □ dBA 75.5 □ dB Noise reduction provided by barrier(s): 12.4 □ dBA 8.0 □ dB										
						nd with					
Source		dBA	$\frac{dB}{dB}$ 63	125	250	500	1k	2k	4k	8k	
Komatsu WA 50	0 FEL w/ barrier w/out barrier		67.5□ 61 [75.5□ 67 [56□ 64□	55□ 66□	52□ 65□	46 □ 62 □	36□ 56□	25□ 48□	
Receiver		X	Y	Z							
Residence 7 - Ge	lfand Residence	$\overline{0}$	$\overline{0}$	$\frac{Z}{5\square}$							
		So	urce Coord	dinates		Barrio	er Coor	dinates]	rees	
Source Name		X	<u>Y</u>	\underline{Z}	X		Y	\underline{Z}		ft	
Komatsu WA 50	0 FEL	150□	$\overline{0}$	-2	10	00 🗆	$0\Box$	7		$\overline{0}$	

Date:	7/27/00				Proje	ct Num	ber: 1	59916				
Project Name:	Daybreak Mining S	ite - Ame	ended Minin	g Plan	NEngin	neer:y	K	GS				
Comments:	Prediction to determ to meet County 5 dI is 12' below grade in	3 change	rule with no	reduct	tion of	FEL no	oise and	l assum	ing the		eus Re	
Number of source	es: 1□				Temp	erature	: 50□					
Number or receive			Humidity: 70□									
Maximum reduct	tion provided by barri	ier: 24□										
				Refer	ence L	evels						
Source	Ref Dis	t dBA	lB 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	$0 \text{ FEL} \qquad \boxed{100}$	$\overline{73.3}$ \square $\overline{7}$		 76□		$\overline{70}$	 69□	 66□	 61□	 53□		
Total noise level Total noise level	Receiver 1: Residence 8B - Dorcheus Residence Total noise level with barrier(s): 54.4 dBA 65.9 dB Total noise level without barrier(s): 69.5 dBA 75.5 dB Noise reduction provided by barrier(s): 15.1 dBA 9.7 dB											
					with a							
Source		dBA d	lB 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	0 FEL w/ barrier	54.4□ €	55.9□ 60□	64□	53□	53□	$49\square$	$42\square$	$33\square$	$24\square$		
	w/out barrier	69.5□ 7	75.5□ 67□	72 □	64□	66□	65□	62□	56□	48□		
Receiver Residence 8B - I	Oorcheus Residence	$\frac{\mathrm{X}}{\mathrm{0}}$	$\frac{\mathrm{Y}}{\mathrm{0}}$	$\frac{Z}{5}$								
		Sou	rce Coordir			Dorri	or Coor	dinates	, 7	Frans		
Source Name		X	Y	Z	X		Y	Z		Γrees ft		
	Λ ΕΕΙ	$\frac{\Lambda}{150}$	$\frac{1}{0}$	$\frac{2}{-2}$		00 🗆	$\frac{1}{0}$		-)□			
Komatsu WA 50	UFEL	130	U	- 2	10	JU 🗆	U	10	J	$0\Box$		

Date:	7/27/00				Projec	ct Num	ber: 1	59916						
Project Name:	Daybreak Mining S	Daybreak Mining Site - Amended Mining Plan NEngineer:y KGS Prediction to determine barrier height required around Phase 3 pit for Residence 8 (Dorcheus Resi												
Comments:	Prediction to determ to meet County 5 dl is 12' below grade in	3 change	rule with n	o reduct	tion of	FEL no	oise and	l assum	ing the		us Resi			
Number of sourc	es: 1□				Temp	erature	: 50□							
Number or receiv		Humidity: 70□												
Maximum reduct	tion provided by barr	ier: 24□												
					ence L									
Source	Ref Dis	$\frac{dBA}{d}$	B 63	125	250	500	1k	2k	4k	8k				
Komatsu WA 50	0 FEL 100□	73.3 🗆 7	9.1□ 71□	76□	68□	$70\square$	69□	66□	61□	53□				
Total noise level Total noise level	Receiver 1: Residence 8 - Dorcheus Residence Total noise level with barrier(s): 54.2 □ dBA 63.0 □ dB Total noise level without barrier(s): 63.2 □ dBA 69.4 □ dB Noise reduction provided by barrier(s): 9.1 □ dBA 6.4 □ dB													
C		10 4 1	D (2		with a				41	01				
Source			B 63	125	<u>250</u>	500	1k	<u>2k</u>	4k	8k				
Komatsu WA 50			$3.0 \square 56 \square$	61 🗆	52□	53 🗆	50□	44 🗆	34□	22 🗆				
	w/out barrier	63.2 🗆 6	9.4□ 61□	66□	58□	60□	59□	56□	48□	40□				
Receiver		X	<u>Y</u>	<u>Z</u>										
Residence 8 - Do	rcheus Residence	$0\square$	$0\Box$	$5\square$										
		Sou	rce Coordii	nates		Barrio	er Coor	dinates		Trees				
Source Name		X	Y	Z	X		Y	\underline{Z}		ft				
Komatsu WA 50	0 FEL		$\overline{0}$	<u>-2</u> □	16	50□	$\overline{0}$	$\frac{1}{7}$		$\overline{0}$				

Date:	7/27/00				Projec	ct Num	ber: 1	59916				
Project Name:	Daybreak Mining S	ite - Ame	nded Minin	ng Plan	NEngin	neer:y	K	GS				
Comments:	Prediction to determ to meet County 5 di is 12' below grade i	B change	rule with no	o reduct	tion of	FEL no	oise and	l assum	ing the		eus Resi	
Number of sourc	es: 1□			Temperature: 50 □								
Number or receiv		Humidity: 70□										
Maximum reduct	tion provided by barr	ier: 24⊔										
Reference Levels												
Source	Ref Dis	$t \stackrel{\text{dBA}}{=} \underline{d}$	B 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	0 FEL 100□	73.3 🗆 7	9.1□ 71□	76□	68□	70□	69□	66□	61□	53□		
Total noise level	Receiver 1: Residence 8 - Dorcheus Residence Total noise level with barrier(s): 54.3 □ dBA 64.9 □ dB Total noise level without barrier(s): 66.9 □ dBA 73.0 □ dB Noise reduction provided by barrier(s): 12.6 □ dBA 8.1 □ dB											
Carres		TD V =	ID 62		with a				41.	01-		
Source	0 PP7 /1 :		$\frac{1}{1}$ $\frac{63}{1}$	$\frac{125}{62}$	$\frac{250}{53}$	$\frac{500}{500}$	$\frac{1k}{10}$	$\frac{2k}{12}$	$\frac{4k}{2a}$	$\frac{8k}{2}$		
Komatsu WA 50	0 FEL w/ barrier w/out barrier		54.9□ 59□ 73.0□ 65□	63 □ 70 □	53 □ 62 □	53 □ 64 □	49□ 63□	43 □ 59 □	33 □ 53 □	22□ 45□		
	W/Out Dairiei	00.9 /	3.00 030	/∪⊔	02	04 🗆	03 🗆	39	33 L	43 🗆		
Receiver		X	Y	Z								
Residence 8 - Do	orcheus Residence	$\overline{0}$	$\overline{0}$	5□								
		Sou	rce Coordin	nates		Barrie	er Coor	dinates		Trees		
Source Name		X	Y	$\frac{Z}{Z}$	X		Y	Z		ft		
Komatsu WA 50	0 FEL	$\overline{200}$	$\overline{0}$	<u>-2</u> □	$\frac{-}{12}$	20 🗆	$\overline{0}$	9		$\overline{0}$		

Date:	7/27/00				Projec	ct Num	ber: 1	59916			
Project Name:	Daybreak Mining Si	ite - Ameno	ded Minin	g Plan	NEngin	eer:y	K	GS			
Comments:	Prediction to determ to meet County 5 dE is 12' below grade in	3 change ru	ile with no	reduct	tion of I	FEL no	oise and	l assum	ing the	•	ord Re
Number of source Number or receiv Maximum reduct		er: 24□			Temp Humi	erature dity:	e: 50□ 70□				
				Refer	ence Le	evels					
Source	Ref Dist	t dBA dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 500	$0 \text{ FEL} \qquad 100 \square$	73.3 🗆 79	.1 🗆 71 🗆	76□	68□	70□	69□	66	61	53□	
	Residence 8D - Crawith barrier(s): without barrier(s): provided by barrier(s)	54.0□dB 63.2□dB	A 62. A 69.	.9□dB .4□dB .5□ dB							
				Level	with a	nd with	out ba	rrier			
Source		dBA dB	63	125	250	500	1k	2k	4k	8k	
Komatsu WA 500		54.0□ 62		61□	52□	52□	49□	$43\square$	$33\square$	$22\square$	
	w/out barrier	63.2□ 69	.4□ 61□	66□	58□	60□	59□	56□	48□	$40\square$	
Receiver Residence 8D - C	Crawford Residence	$\frac{X}{0}$	$\frac{\mathrm{Y}}{\mathrm{0}}$	$\frac{Z}{5}$							
		Sourc	e Coordin	ates		Barrio	er Coor	dinates	;]	Γrees	
Source Name		X	Y	<u>Z</u>	X		Y	\underline{Z}	_	ft	
Komatsu WA 500	0 FEL	300□	$0\square$	-2□	26	50□	$0\square$	3		$0\square$	

Date:	7/27/00				Projec	et Num	ber: 1	59916							
Project Name:	Daybreak Mining Si	ite - Amen	ded Minin	g Plan	NEngin	eer:y	K	GS							
Comments:	Prediction to determine barrier height required around Phase 3 pit for Residence 8D (Crawford Retornet County 5 dB change rule with no reduction of FEL noise and assuming the FEL is 12' below grade in NE corner of pit 4- Saved in file 159916-pit3FEL-12.env														
	Number of sources: 1□ Number or receivers: 1□ Maximum reduction provided by barrier: 24□						Temperature: 50 □ Humidity: 70 □								
				Refer	ence Le	evels									
Source	Ref Dist	t dBA dE	63	125	250	500	1k	2k	4k	8k					
Komatsu WA 500	O FEL $100\Box$	73.3 🗆 79	.1 🗆 71 🗆	7 6□	68 □	$\overline{70}$		66	6 1□						
	Residence 8D - Crawith barrier(s): without barrier(s): provided by barrier(s)	53.6□dB 63.2□dB	A 62. A 69.	.8□dB .4□dB '□ dB											
~					with a					0.1					
Source		dBA dE		125	250	500	1k	2k	4k	8k					
Komatsu WA 500		53.6 62		60 🗆	52□	52□	49 □	43 🗆	33□	21 🗆					
	w/out barrier	63.2□ 69	.4□ 61□	66□	58□	60□	59□	56□	48□	40□					
Receiver Residence 8D - C	crawford Residence	$\frac{\mathrm{X}}{\mathrm{0}}$	$\frac{\mathrm{Y}}{\mathrm{0}}$	$\frac{Z}{5\Box}$											
		Sour	ce Coordin			Rarrie	er Coor	dinates	. Т	rees					
Source Name		X	Y	Z	X		Y			ft					
Komatsu WA 500) FEL	300□	$\overline{0}$	<u>-2</u> □	21	0	$\overline{0}$	6		$\overline{0}$					

Date:	7/27/00 Project Number: 159916											
Project Name:	Daybreak Mining S	lite - Ame	nded Minin	g Plan	NEngin	neer:y	K	GS				
Comments:	Prediction to determ to meet County 5 di is 12' below grade i	B change	rule with no	o reduct	tion of	FEL no	oise and	l assum	ing the	•	Reside	
Number of source Number or receive Maximum reduce		ier: 24□	Temperature: 50 ☐ Humidity: 70 ☐ er: 24 ☐									
Reference Levels												
Source	Ref Dis	t dBA	lB 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	0 FEL 100□	$\overline{73.3}$ \square $\overline{7}$	<u>7</u> 9.1□ 71□	76 □		70 □			<u></u> 61□			
Receiver 1: Residence 9 - Hanger Residence Total noise level with barrier(s): 53.7□dBA 61.3□dB Total noise level without barrier(s): 60.6□dBA 66.9□dB Noise reduction provided by barrier(s):6.9□dBA 5.6□dB												
						nd with						
Source		$\frac{dBA}{dBA}$	IB 63	125	250	500	1k	2k	4k	8k		
Komatsu WA 50	0 FEL w/ barrier		51.3□ 54□	59□	50□	52□	50□	44 🗆	34□	23 □		
	w/out barrier	60.6□ 6	66.9□ 59□	64□	56□	58□	57□	53□	45□	36□		
Receiver		X	Y	<u>Z</u>								
Residence 9 - Ha	inger Residence	$\overline{0}$	$\overline{0}$	<u>5</u> □								
		Sou	rce Coordin	nates		Barrie	er Coor	dinates]	rees		
Source Name		X	Y	$\frac{Z}{}$	X	_	Y	$\frac{Z}{Z}$		ft		
Komatsu WA 50	0 FEL	$\overline{400}$	$\overline{0}$	-2 □	22	20 🗆	$0\Box$	5		0 🗆		